



February 8, 2019

Revised April 24, 2019

Project No. 180127E001

Ron Beresky
8100 SE 48th Street
Mercer Island, Washington 98040

Subject: Revised Segmental Block Retaining Wall Design
8100 SE 48th Street
Mercer Island, Washington

Reference: Geotechnical Engineering Report
New Retaining Wall Feasibility
8100 SE 48th Street
Mercer Island, Washington
Date: October 2, 2018

Dear Mr. Beresky:

As requested, Associated Earth Sciences, Inc. (AESI) is pleased to present the attached revised design details, sections, elevations (Figures 1 and 2) and associated calculations for a new terraced Allan Block™ mechanically stabilized earth (MSE) wall system for your property. Our latest design reflects the use of three terraced gravity walls to be constructed with a minimum 2-foot-wide section of “no fines concrete” with a Classic Allan Block facing as shown on Figures 1 and 2, attached.

Our work has been performed in accordance with our proposal, dated October 2, 2018. We have revised our original drawings transmitted to you on October 2, 2018, to reflect design changes based on multiple meetings with your wall construction contractor, Western Landscaping and Pavers. We understand that the City of Mercer Island must approve our design prior to construction.

Global slope stability modeling was completed on critical Section B-B' (Figure 2) utilizing GeoStudio 2018 R2 software. This program accepts inputs that we provide based on published geologic mapping, available topographic information, our engineering experience in similar soils, and other sources. The model identifies critical slope failure surfaces that are then analyzed to determine

their factor of safety against failure under the input conditions. The factor of safety is a ratio between forces driving slope failure and forces resisting slope failure. A factor of safety of 1.0 is indicative of a failure surface with driving and resisting forces that are equal, and a slope failure is predicted. Factors of safety that exceed 1.0 indicate that resisting forces are greater than driving forces. For new construction, a static factor of safety of 1.5 or more is considered typical. Under design earthquake loads, pseudostatic (dynamic) factors of safety of 1.1 are required for work within the City of Mercer Island. For this project, we modeled the design earthquake using an acceleration of 0.30g or one-half of the Peak Ground Acceleration (PGA) as determined using the United States Geological Survey's (USGS's) online Design Maps tool, which is consistent with local standards of practice for slope modeling applications, in our opinion.

Existing topography inputs for slope stability modeling were developed based on a "Topographic Survey" by Harmsen and Associates, dated May 17, 2018. Slope stability modeling requires soil strength parameters. For this project, the site sediments that were modeled included surficial colluvium and the underlying very dense pre-Olympia till encountered at a depth of approximately 3 feet in two hand borings excavated on March 21, 2019, at the locations shown on Figure 1. Both hand borings encountered 3 feet of loose, silty sand with abundant organic material and roots (colluvium) overlying very dense, gray, silty sand with gravel (native pre-Olympia till). Both hand borings were terminated at a depth of 4 feet in the till due to refusal. We did not generate soil logs of the hand borings.

The model geometry is shown on Figure SS1, attached. For Sections B-B', the footing loads for the proposed deck and existing home were modeled as direct line loads applied at the locations shown on Figure 2 and the slope stability output Figures SS1 through SS4, attached.

Soil parameters used for our stability analyses are summarized on the slope stability model output Figures SS1 through SS4, attached. The composite "no fines concrete" with block facing was modeled with a conservative cohesion value of 2,000 pound per square foot (psf) that would be resistant to internal shearing. Soil parameters used to model the pre-Olympia glacial till deposits are based on the soils encountered in our borings (refer to our referenced geotechnical report), established published correlations, and previous experience with similar soils in the Puget Sound area. The parameters used represent mid-range values of the published information as shown in "Geotechnical Properties of Geologic Materials, Engineering Geology in Washington, Volume I, Bulletin 78, 1989" by Kowalski, J.W., Schwarz, S.D., and Tubbs, D.W.

Based on our slope stability modeling, a minimum static factor of safety of 1.5 was generated with the failure circle primarily involving the surficial colluvium (Figure SS2). Under seismic conditions, the minimum factor of safety involving failure circles in the pre-Olympia till is 1.1 (Figure SS3). Based on the modeling, it is likely that surficial land sliding similar to what has occurred on the property in the past could occur during a design level earthquake (Figure SS4). However, these failure circles are confined to the surface colluvium below the proposed new walls. Therefore, it is imperative that the lowest tier of the wall system is founded in competent, undisturbed pre-

Olympia till and that the wedge of soil at the toe of the proposed walls must be constructed in accordance with the sections shown on Figures 1 and 2 with either sufficiently compacted crushed rock or concrete.

The attached design calculations for Sections A-A' through C-C' were completed utilizing the software program AB Walls™ version 19.00.08 - 4/15/2019. Our latest design reflects the use of three terraced gravity walls to be constructed with a minimum 2-foot-wide section of "no fines concrete" with a Classic Allan Block facing as shown on Figures 1 and 2, attached. AB Walls™ software output for Sections A-A' through C-C' is also attached to this letter.

We modeled the loading from the upper gravity walls as a 600 psf uniform surcharge pressure starting 4 feet behind the lower-most wall. For Sections B-B' and C-C', the deck foundation was superimposed on the upper terrace loads as a 1,000 psf line load. On Section B-B', this line load does not appear to influence the loading on the base wall because of its positioning a minimum horizontal distance of 12 feet from the bottom wall, although it was included in the calculation. Section C-C' also includes a surcharge pressure for the proposed 2H:1V (Horizontal:Vertical) slope to be constructed above the wall in addition to the deck foundation load (Figure 2). As demonstrated by the AB Walls software output, the proposed configuration demonstrates adequate factors of safety for sliding and overturning under static and seismic (earthquake) loading conditions.

Our design is predicated on AESI being present onsite full-time during wall construction to verify bearing soils have been exposed in the foundation cut for all terraces, during no fines concrete and drainage installation, and during installation during backfill of the area at the toe of the new wall system. All soils excavated from the site must be removed from the site and specifically not placed on the slope beneath the new walls. In addition, surface and groundwater must be controlled at all times and must not be allowed to flow over the on- or off-site slopes under any circumstances. If utilities are identified within the slope that will conflict with our design, we should be notified prior to commencement of any further work. All work must be performed during the dry summer months between May and September unless specific permission is granted by the City of Mercer Island.

We appreciate the opportunity to be of continued service to you on this project. Should you have any questions regarding the attached documents, please call us at your earliest convenience.

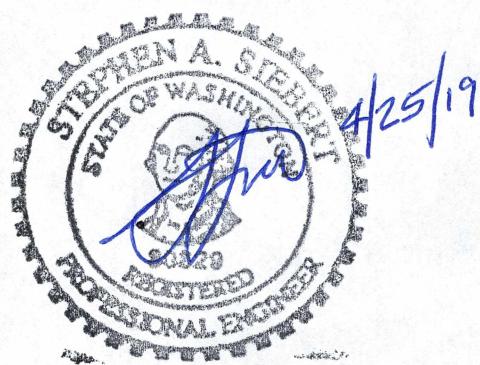
Sincerely,
ASSOCIATED EARTH SCIENCES, INC.
Kirkland, Washington

Susan G. Beckham

Susan G. Beckham, P.E.
Senior Geotechnical Engineer

Bruce L. Blyton

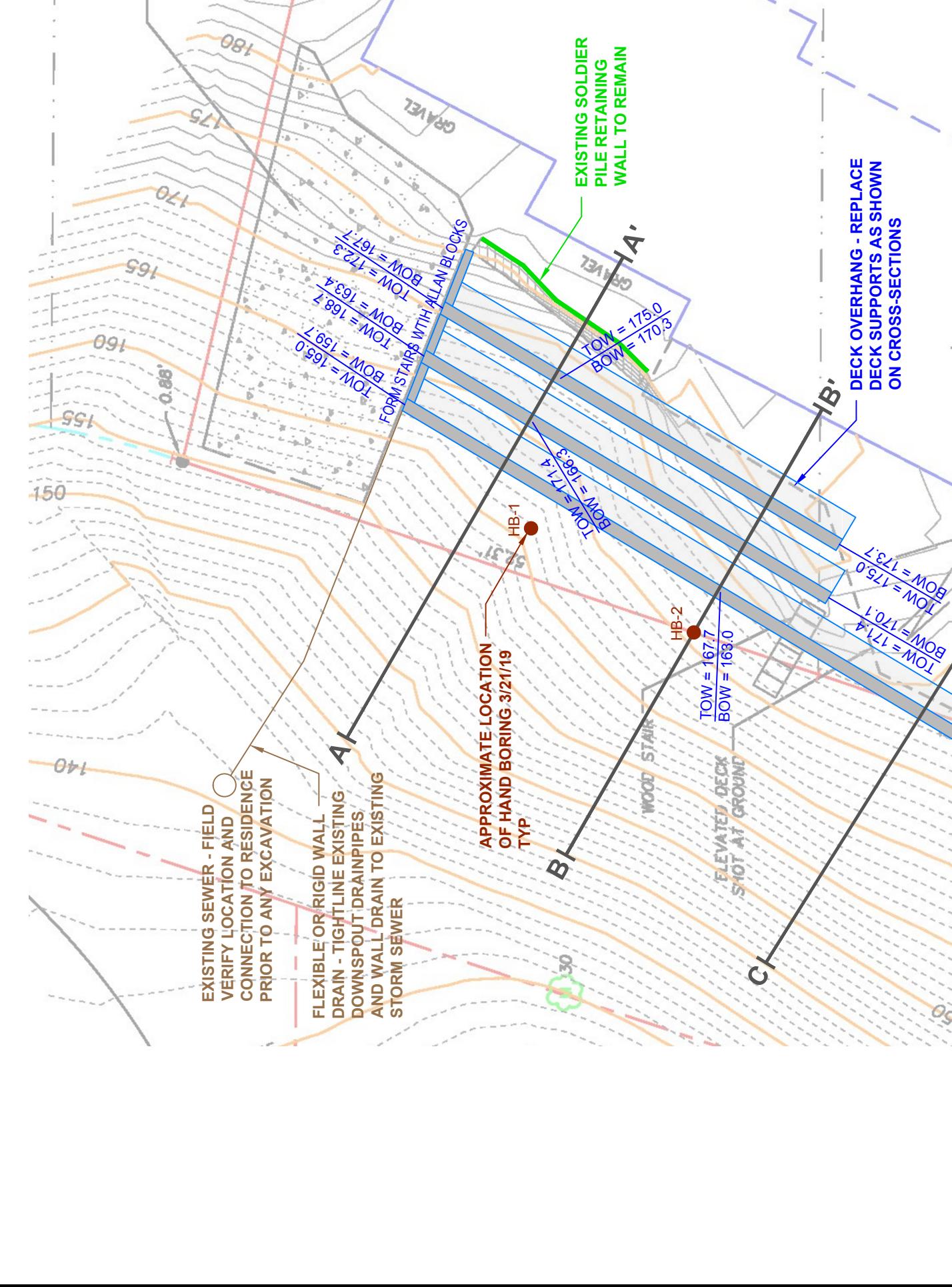
Bruce L. Blyton, P.E.
Senior Principal Engineer

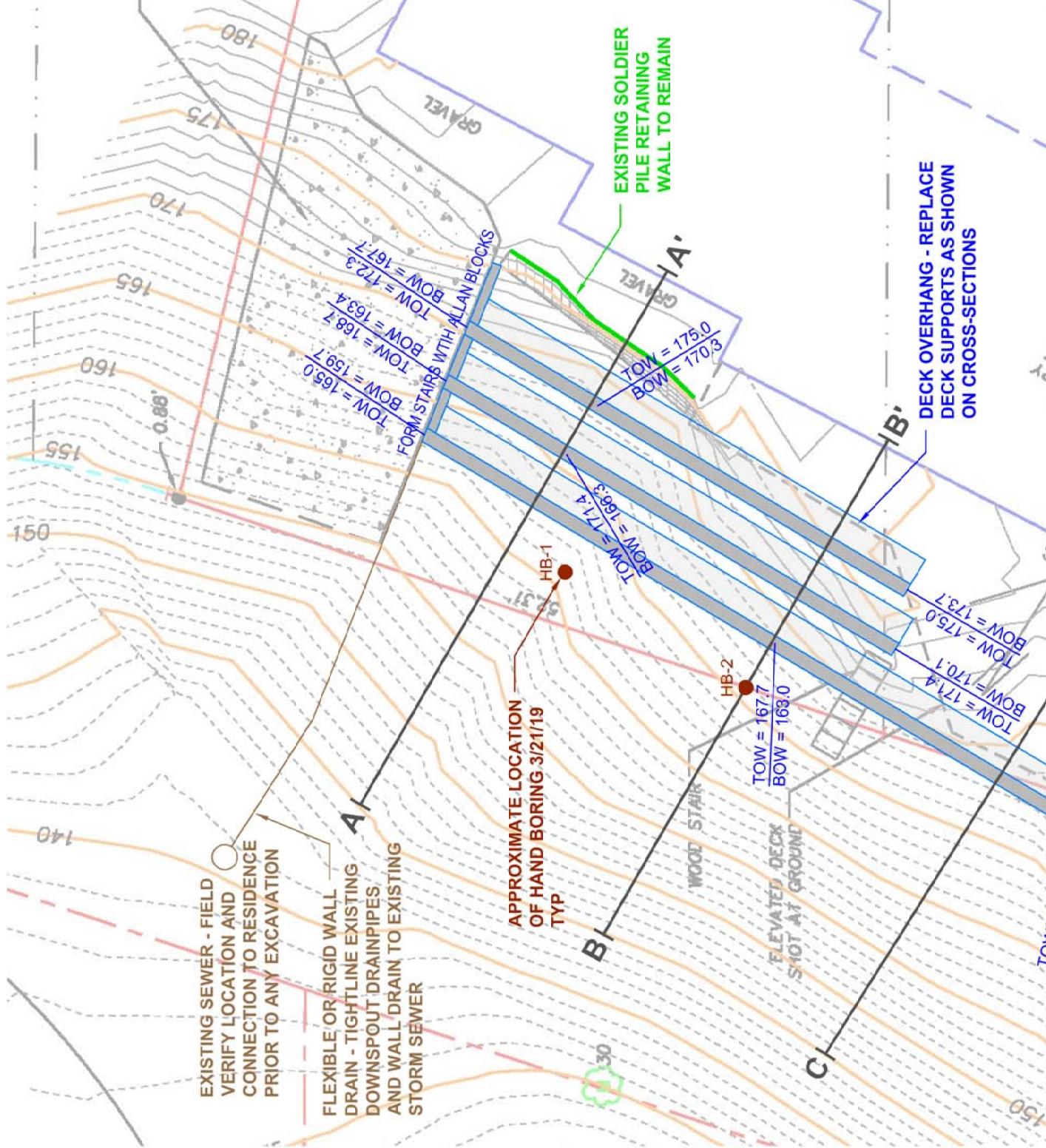


Stephen A. Siebert, P.E.
Associate Geotechnical Engineer

Attachments: Figures 1 & 2: Allan Block Wall, Beresky Residence -
8100 SE 48th Street, Mercer Island, Washington
Figures SS1-SS4: Slope Stability Output
AB Walls™ computer analysis output Sections A-A' through C-C'

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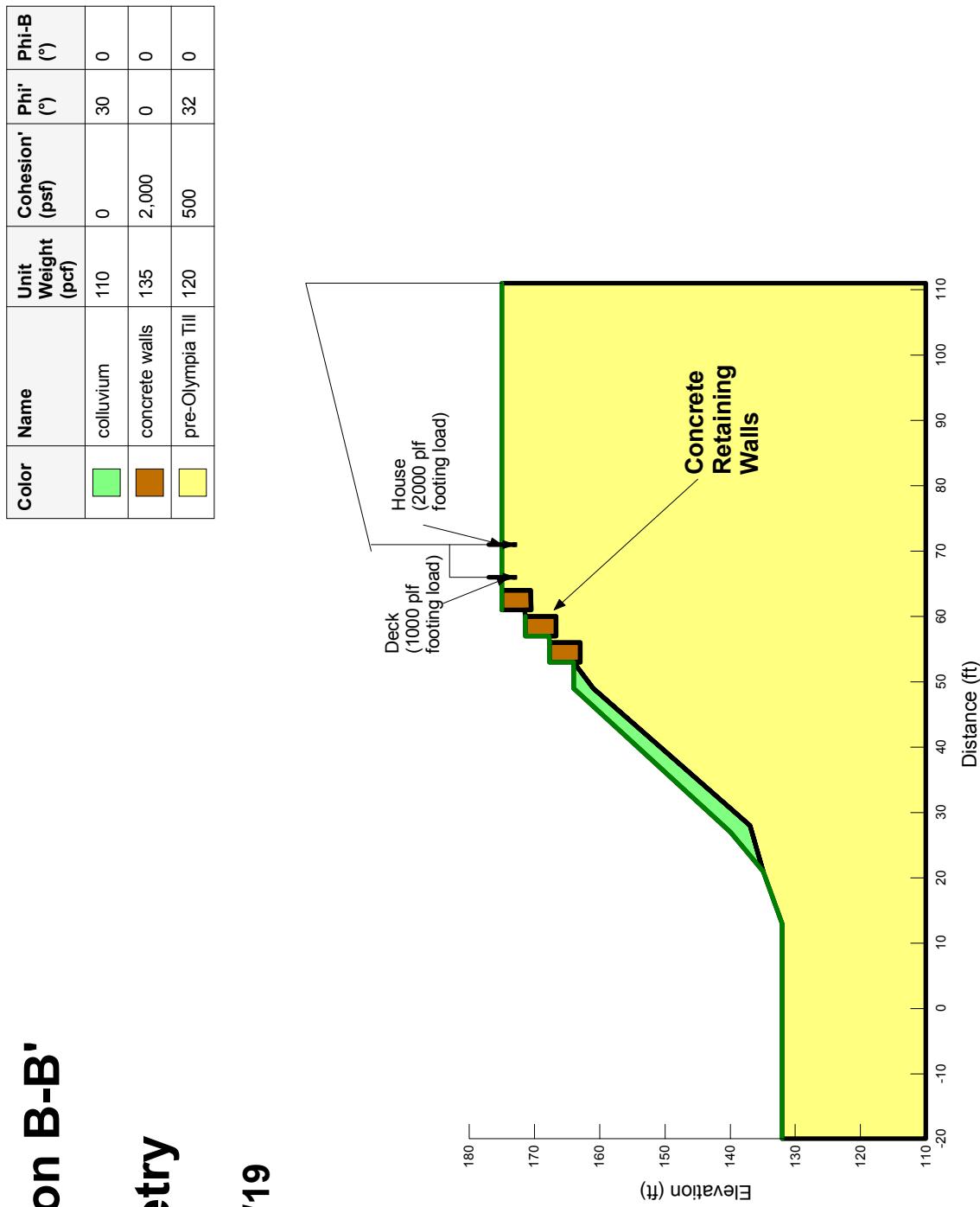
Beresky Retaining Walls

180127E001

Critical Section B-B'

Slope Geometry

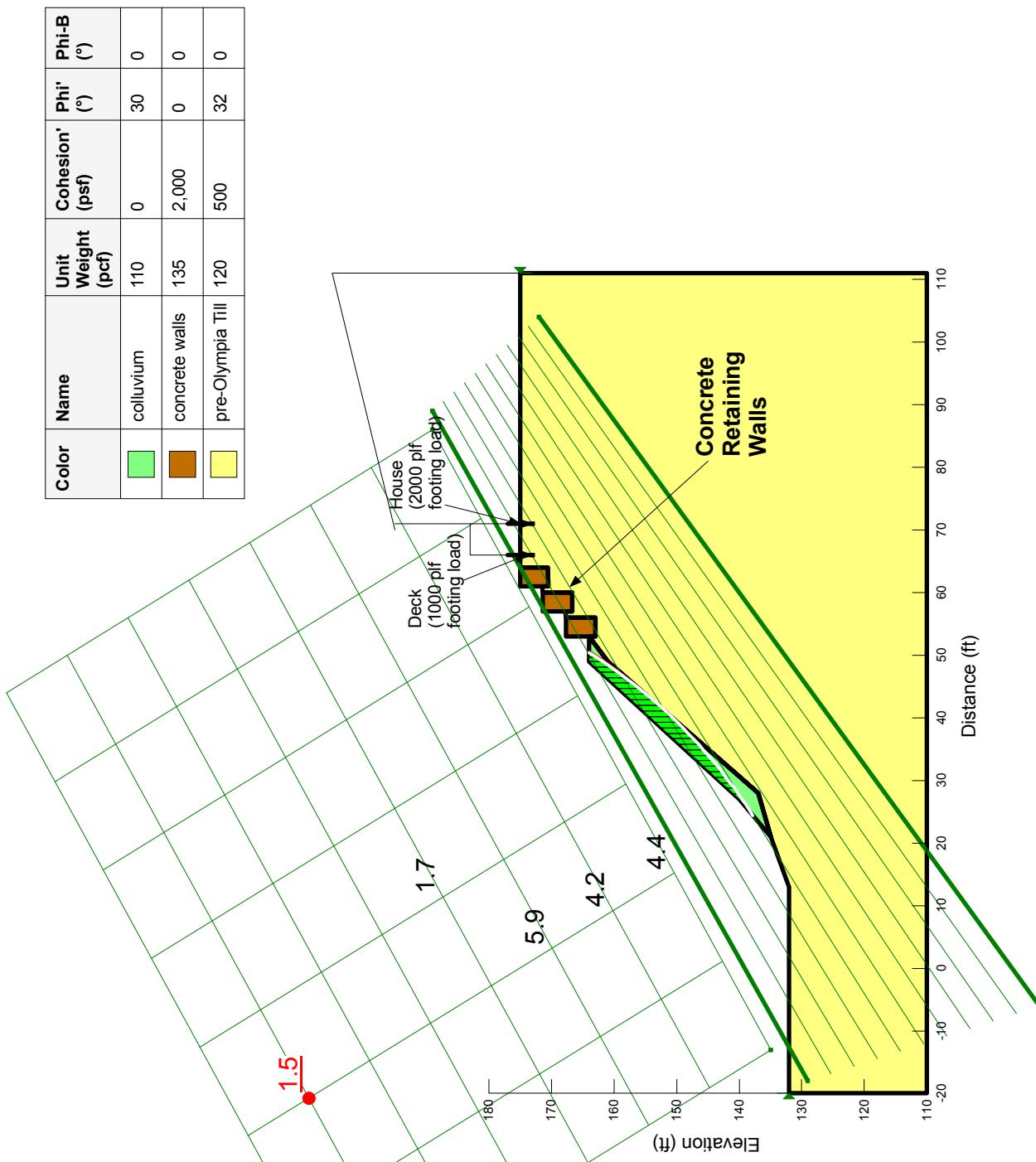
Figure SS1 - 4/19/19



Beresky Retaining Walls
180127E001
Critical Section B-B'

Static Conditions

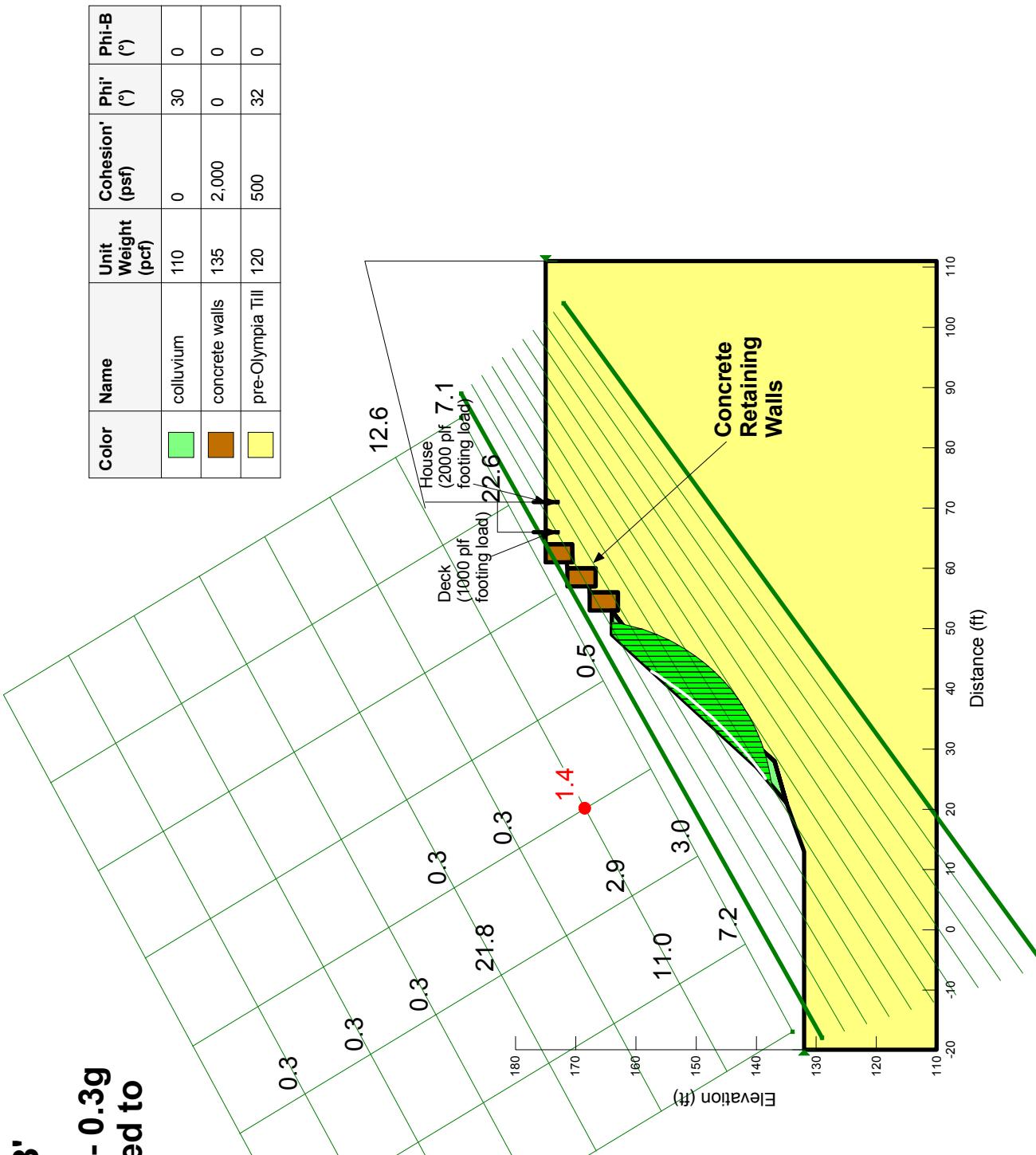
Figure SS2 - 4/19/19



Beresky Retaining Walls
180127E001
Critical Section B-B'

Seismic Conditions - 0.3g
All FOS < 1.1 confined to
colluvium

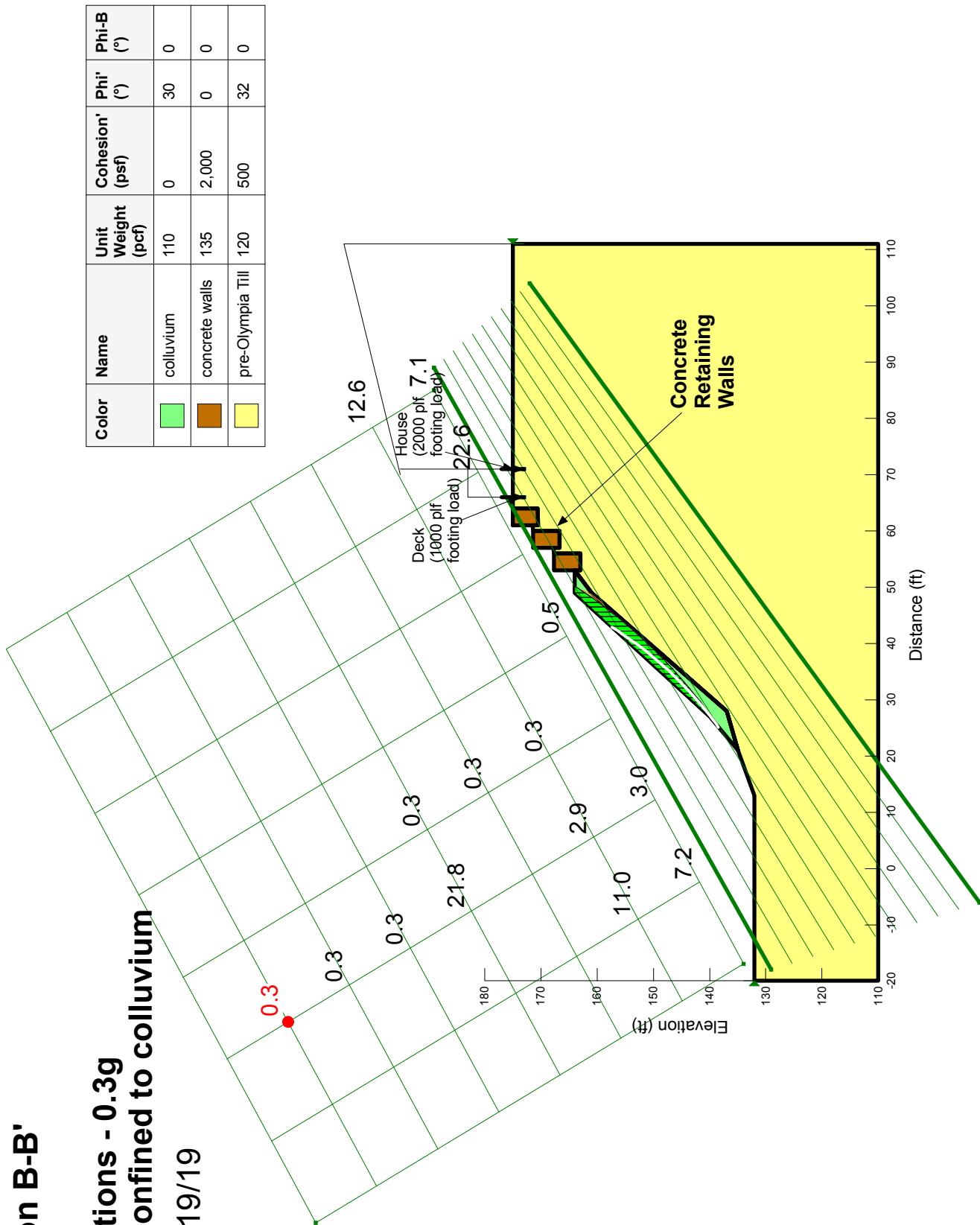
Figure SS3 - 4/19/19



**Beresky Retaining Walls
180127E001
Critical Section B-B'**

Seismic Conditions - 0.3g
All FOS < 1.1 confined to colluvium

Figure SS4 - 4/19/19



Wall Design Variables	
AB Classic	Total Panel Height 5.17 ft Block Height 0.646 ft Angle of Setback 6 Deg. Depth of Block 0.98 ft Length of Block 1.47 ft
Surcharge Parameters	600 psf Dead Load (@ 4 ft) (Distance measured from toe of wall)
Safety Factors Static External	Actual Sliding = 0.3 1.53 >= 1.5 Actual Overturning 2.6 >= 2
Safety Factors Seismic External	Peak Ground Acceleration = 0.3 Actual Sliding 1.16 >= 1.125 Actual Overturning 1.84 >= 1.5
Infill Soil	Friction Angle 75 Deg. Unit WT 110 psf
Retained Soil	Friction Angle 32 Deg. Unit WT 120 psf
Foundation Soil	Friction Angle 32 Deg. Unit WT 120 psf Cohesion 0 psf
Bearing Capacity	Factor of Safety 4.37 Sigma ult - 6727.47 psf Sigma max - 1539.12 psf
Internal Compound Stability	ics not calculated
Wall Rock Requirements	Variable Depth Bottom 4.52 ft Height 1 ft Depth 1 ft

Project Name: Beresky Residence
Section: Section A-A
Location: Mercer Island, WA
Wall Number: 180127E001
Designer: AESI
Project Number: 180127E001
Date: 4/18/19

Section A-A

Base Information:
Base Width: 2 ft
Base Depth: 0.5 ft
Base From Toe: 0.5 ft

Allan Block Disclaimer:
Allan Block provides this software as a service for its clients. The sole purpose of this software is to assist engineers in the design of mechanically stabilized earth walls. The software uses engineering principles and methods to calculate the stability of the wall. The software does not guarantee the results will be correct or safe. The user is responsible for the proper use and interpretation of the results. ALLAN BLOCK CORPORATION, its officers, employees, agents, and contractors do not assume any liability or responsibility for damage which may result from the property and accuracy of input parameters and to review and verify the correctness of the results. ALLAN BLOCK CORPORATION, its officers, employees, agents, and contractors do not assume any liability or responsibility for damage which may result from the use or misuse of this software.

This software only considers internal, external and internal compound stability of the reinforced composite mass. The internal compound stability calculations are limited to an evaluation zone above the base material and back further than $2 \cdot H + L$, where H is the height of the wall and L is the distance from the toe to the center of the reinforcement. This program does not address global stability below the base material and beyond this limit. It is the responsibility of the engineer to determine if the wall is stable under all conditions. The software is intended to be used as a tool to evaluate the potential for failure and to determine the required reinforcement to prevent such failure. The software is not intended to be used as a substitute for professional judgment or proper water management, and all potential modes of failure within the segment retaining wall evaluation zone. The geotechnical engineer contracted by the owner should provide a full global stability opinion of the site including the effects on the segmental retaining wall.

AB Wall contains DEFAULT values for all data inputs that the user MUST change or verify as appropriate for the project conditions being analyzed. These DEFAULT values do NOT ensure a conservative design for any site condition. This final design must provide for proper wall drainage to prevent the buildup of hydrostatic pressures over the service life of the structure. In the event additional analyses are required, the user is responsible for performing those analyses and consulting with a registered professional engineer. All analyses must be performed in accordance with the applicable codes and standards of the jurisdiction. Settlement potential and wall deflections for the proposed structure are not included in this software. These additional potential failure modes should be evaluated by the engineer prior to initiating wall construction and may require site inspection by the on-site soil engineer.

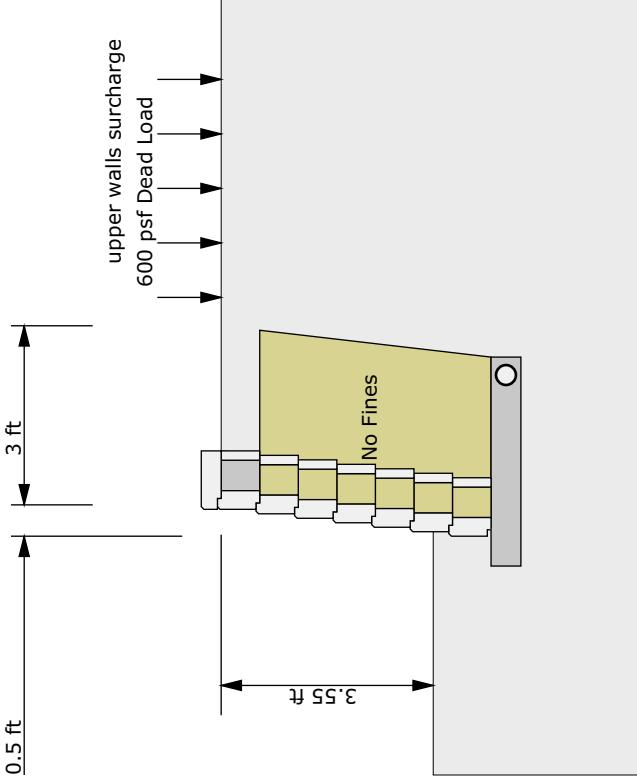
MATCAD files for hand calculations to support the software's consideration of internal, external and internal compound stability of the reinforced composite mass are provided on the software disc. These files are to be configured so that the engineer of record can evaluate the output of the software. Individual equations may be altered at the discretion of the engineer of record.

Project Number: 180127E001
 Wall Number: Mercer Island, WA
 Location: Section B-B,
 Project Name: Beresky Residence
 Designer: AESI
 Date: 4/18/19

v.19.0

Page 1 of 1

Wall Design Variables	
AB Classic	Total Panel Height 4.52 ft Block Height 0.646 ft. Angle of Setback 6 Deg. Depth of Block 0.98 ft Length of Block 1.47 ft
Surcharge Parameters	600 psf Dead Load @ 4 ft 1000 psf Dead Load: 12 ft - 13 ft <small>(Distance measured from toe of wall)</small>
Safety Factors Static External	Peak Ground Acceleration = 0.3 Actual Sliding $1.68 \geq 1.5$ Actual Overturning $3.34 \geq 2$
Safety Factors Seismic External	Actual Sliding $1.27 \geq 1.125$ Actual Overturning $2.34 \geq 1.5$
Infill Soil	Friction Angle 75 Deg. Unit WT 11.0 pcf
Retained Soil	Friction Angle 32 Deg. Unit WT 12.0 pcf
Foundation Soil	Friction Angle 32 Deg. Unit WT 12.0 pcf Cohesion 0 psf
Bearing Capacity	Factor of Safety 8.3 Sigma_ult = 8709.49 psf Sigma_max = 1049.35 psf
Internal Compound Stability	ics not calculated
Wall Rock Requirements	Variable Depth Height Bottom 3.87 ft Depth 1 ft



The diagram illustrates the cross-section of the AB Classic wall. It shows a vertical wall with a height of 3 ft and a base width of 3.55 ft. The wall is supported by a foundation soil layer. Above the foundation, there is a 'No Fines' soil layer. The diagram also indicates an 'upper walls surcharge' with a force of 600 psf Dead Load applied over the top 4 ft of the wall height.

Base Information:
 Base Width: 3.5 ft
 Base Depth: 0.5 ft
 Base From Toe: 0.5 ft

Section B-B'

Allan Block Disclaimer:
 Allan Block does not provide engineering services or advice for its clients. The sole purpose of this software is to assist engineers in the design of Allan Block retaining walls. This software uses evaluation techniques and engineering principles found in the Allan Block Engineering Manual. (Refer to R010 and supporting references.) It is the responsibility of the engineer of record to determine the properity and accuracy of input parameters and to review and verify the correctness of the results. ALLAN BLOCK CORPORATION, USE OR OWNERSHIP OF THIS SOFTWARE DOES NOT ASSUME ANY LIABILITY OR RESPONSIBILITY FOR DAMAGES WHICH MAY RESULT FROM THE USE OF THIS SOFTWARE.

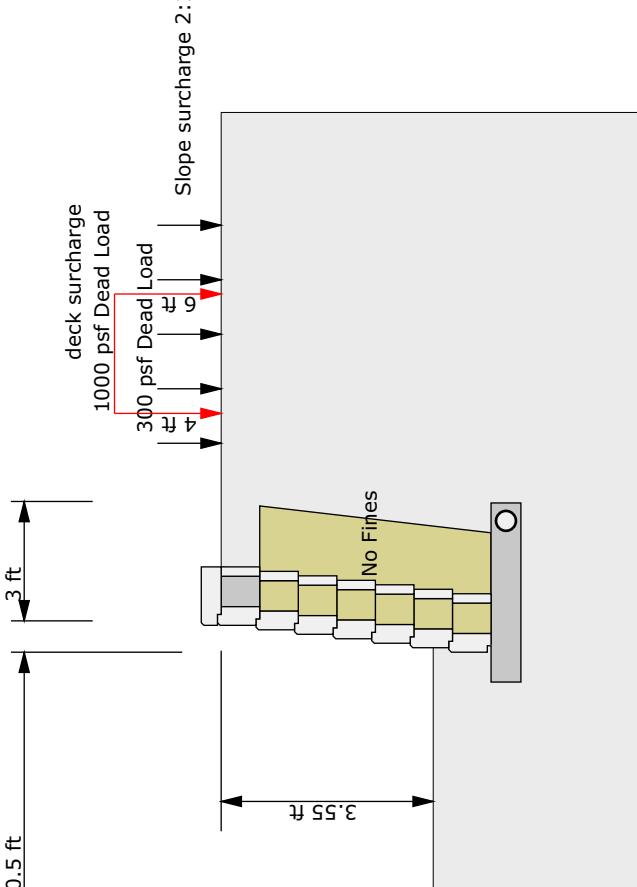
This software only considers internal, external and internal compound stability of the reinforced composite mass. The internal compound stability calculations are limited to an evaluation zone above the base material and back no further than $2 + L_{\text{comp}}$ ft from the toe of the wall. The software does not consider the effects of lateral earth pressure on the overall site stability. It is the responsibility of the owner to insure the global stability is analyzed and determined by the engineer of record. The engineer of record must evaluate the project site for proper water management and all potential modes of failure within the segmental retaining wall evaluation zone. The geotechnical engineering firm contracted by the owner should provide a full global stability opinion of the site including the effects on the segmental retaining wall.

AB Walls contains DEFAULT values for all data inputs that the user MUST change or verify as appropriate for the project conditions being analyzed. These DEFAULT values do NOT ensure a conservative design for any site condition. The final design must provide for the unique characteristics of each site. If the software indicates that the wall is unstable, the engineer of record must determine if the wall is stable in the general wall area, either above or below grade. Any design from this software would be invalid unless otherwise noted by the engineer of record. It is also recommended that an independent assessment of the foundation soil for settlement potential and/or deflections to the proposed structure be performed. Changes in the subsurface conditions are not included in this software. These additional potential failure modes should be evaluated by the engineer of record prior to installing wall components. All installations must conform to the Allan Block Spec Book. (Refer to R010).

MacNAD files for hand calculations is a support the software's consideration of internal, external and internal compound stability of the wall. MacNAD files are not intended to replace the software. Individual equations may be altered at the discretion of the engineer of record can affect the output of the software.

Project Number: 180127E001
 Wall Number: Mercer Island, WA
 Location: Section C-C,
 Project Name: Beresky Residence
 Designer: AESI
 Date: 4/18/19

v.19.0

Wall Design Variables	
AB Classic	Total Panel Height 4.52 ft Block Height 0.646 ft. Angle of Setback 6 Deg. Depth of Block 0.98 ft Length of Block 1.47 ft
Surcharge Parameters	300 psf Dead Load @ 3.5 ft 1000 psf Dead Load: 4 ft - 6 ft <small>(Distance measured from toe of wall)</small>
Safety Factors Static External	Peak Ground Acceleration = 0.3 Actual Sliding $1.54 \geq 1.5$ Actual Overturning $4.53 \geq 2$ $2.63 \geq 1.5$
Infill Soil	Friction Angle 75 Deg. Unit WT 11.0 pcf
Retained Soil	Friction Angle 32 Deg. Unit WT 12.0 pcf
Foundation Soil	Factor of Safety 9.69 Sigma_ult = 8048.82 psf Sigma_max = 830.76 psf
Bearing Capacity	ics not calculated
Wall Rock Requirements	Variable Depth Height Bottom 3.87 ft Depth 1 ft
Internal Compound Stability	
Base Information:	
Base Width: 3 ft	
Base Depth: 0.5 ft	
Base From Toe: 0.5 ft	
AB Classic	
Section C-C'	
	
Allan Block Disclaimer: Allan Block does not provide engineering services or advice for its clients. The sole purpose of this software is to assist engineers in the design of Allan Block products. This software uses evaluation techniques and engineering principles found in the Allan Block Engineering Manual. (Refer to R010 and supporting references.) It is the responsibility of the engineer of record to determine the properity and accuracy of the results. ALLAN BLOCK CORPORATION, INC. OR ANY OF ITS AFFILIATES DO NOT ASSUME ANY LIABILITY OR RESPONSIBILITY FOR DAMAGES WHICH MAY RESULT FROM THE USE OF THIS SOFTWARE.	
This software only considers internal, external and internal compound stability of the reinforced composite mass. The internal compound stability calculations are limited to an evaluation zone above the base material and back no further than $2 \times H + L_c$. The limits for internal compound stability are determined by the overall site stability. If the overall site is stable, the limits for internal compound stability are determined by the foundation soil. If the overall site is unstable, the limits for internal compound stability are determined by the foundation soil. The engineer of record must evaluate the project for proper water management and all potential modes of failure within the segmental retaining wall evaluation zone. The geotechnical engineering firm contracted by the owner should provide a full global stability opinion on the site including the effects on the segmental retaining wall.	
AB Walls contains DEFAULT values for all data inputs that the user MUST change or verify as appropriate for the project conditions being analyzed. These DEFAULT values do NOT ensure a conservative design for any site condition. The final design must provide for the worst case scenario. If the software indicates that the wall is unstable, the engineer of record must determine if the wall is situated in to the general wall area, either above or below grade. If this software would indicate instability otherwise noted by the engineer of record. It is also recommended that an independent assessment of the foundation soil for settlement potential and/or deflections to the proposed structure be performed. Changes in the subsurface conditions are not included in this software. These additional potential failure modes should be evaluated by the engineer of record prior to initiating wall construction. All installations must conform to the Allan Block Spec Book. (Refer to R010).	
RasterCAD files for hand calculations is a support the software's consideration of internal, external and internal compound stability of the wall. The output of the software, individual equations may be altered at the discretion of the engineer of record can ever affect the output of the software.	