

# MEMORANDUM

Project No. 200433

March 19, 2021

To: Matthew Randish, Sun Pacific Energy From: Wash drogeoloais 2224 nsed Geo 3/19/2021 En / Mh **Robert Reginald Hanford Robert R. Hanford Eric Marhofer** Senior Geologist Associate Environmental Engineer bhanford@aspectconsulting.com emarhofer@aspectconsulting.com

#### Re: Mercer Island Shell Interim Cleanup Action Plan

Aspect Consulting, LLC (Aspect) has prepared this Interim Cleanup Action Plan (ICAP) for the Mercer Island Shell (Former BP) site (the Site) located at 7833 SE 28th Street on Mercer Island, Washington (the property). Information used to prepare this plan is based on the Remedial Investigation and Feasibility Study Report (RI/FS) completed by Puget Environmental (Puget) dated January 22, 2020 (Appendix A). The RI/FS was prepared to summarize previous investigation results and conclusions and provide recommendation for final cleanup and site closure under the Washington State Model Toxics Control Act (MTCA) Cleanup Regulations adopted by the Washington State Department of Ecology (Ecology) in Chapter 173-340 of the Washington Administrative Code (WAC).

## 1 Purpose

The purpose of this ICAP is to define the objectives of the cleanup activities that will be performed in conjunction with replacement of the gas station infrastructure on the property, identify additional engineering needs to meet MTCA objectives, and make recommendations for the current planning efforts where appropriate to meet those objectives. This ICAP will be used as a roadmap for setting expectations among stakeholders and facilitating insurance coverage for planning, design, and permitting activities considered reasonable and necessary for the cleanup.

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## 2 Chemicals and Media of Concern

The chemicals of concern (COCs) for the Site are based on the occurrence of chemicals positively identified and confirmed at concentrations above MTCA Method A cleanup levels during Puget's remedial investigation (RI). The COCs for the Site include oil-, diesel-, and gasoline-range organics (ORO, DRO, and GRO), benzene, toluene, ethylbenzene, and xylenes (BTEX). Also, while not specifically mentioned in Puget's RI, naphthalene is considered an appropriate COC for this Site. 1,2-dibromoethane (EDB), 1,2-dichloroethane (EDC), methyl tertiary-butyl ether (MTBE), and lead have not been detected at the Site, where sampled for by Puget.

The affected media at the Site includes soil and groundwater. Soil gas and air were not evaluated as part of the RI and remain as potential media of concern. The vapor exposure pathway remains to be evaluated following interim cleanup actions.

# 3 Applicable Cleanup Standards

This section presents the applicable cleanup standards by which evaluation of interim cleanup action will be measured.

## 3.1 Cleanup Levels

Applicable cleanup levels for the affected or potentially affected media at the Site are as follows:

- Soil: MTCA Method A cleanup levels for unrestricted land use.
- **Groundwater:** MTCA Method A cleanup levels for protection of drinking water as a beneficial use.
- Air: MTCA Method B cleanup levels for air. The cleanup levels for air may be adjusted for a commercial use scenario in accordance with 173-340-750 of the WAC as appropriate.

#### 3.2 Points of Compliance

The standard points of compliance for the Site are as follows:

- Soil for protection from direct contact: from ground surface to a depth of 15 feet.
- Soil for protection of groundwater: throughout the Site.
- **Groundwater** *for protection of drinking water*: extending vertically from the uppermost level of the saturated zone to the lowest-most depth potentially affected.
- Ambient and Indoor Air for protection from inhalation: throughout the Site.

When it is not practicable to achieve cleanup levels in soil at the standard points of compliance, the cleanup action may involve containment of hazardous substances. Remedies involving containment may still be determined to comply with cleanup standards, provided:

- 1. The selected remedy is permanent to the maximum extent practicable.
- 2. The cleanup action is protective of human health and the environment.
- **3.** Appropriate institutional controls, including compliance monitoring and periodic reviews, are implemented (173-340-740(6)(f) WAC).

Following the interim cleanup action, an additional feasibility study (FS) may be required to evaluate the potential for containment and/or setting conditional points of compliance.

# 4 Areas Requiring Remediation

The areas requiring remediation at this Site are defined by exceedances of the applicable cleanup standards discussed above for soil and groundwater.

### 4.1 Soil

Given the nature and extent of contamination presented in Puget's RI/FS, soil impacts exceeding Method A cleanup levels is present approximately 3 to 16 feet below ground surface (bgs) near and between the USTs and dispenser islands. These areas are shown in plan and cross-section views on Figures 5 through 8 of the RI/FS.

#### 4.1.1 On-Property

The lateral extent of soil impacts exceeding Method A cleanup levels is shown on Figure 5 in the RI/FS. Given the uncertainty with respect to the lateral extent of soil impacts potentially extending under the existing convenience store building on the property, it may not be practicable in the context of MTCA to fully remove all soil impacts that are above cleanup levels on the property. A shoring system that maximizes flexibility with respect to chasing soil impacts up to and under the building, such as pin piles or micro piles, is recommended to increase the likelihood of successfully achieving cleanup levels on the property.

Pending the results of confirmation soil sampling below the building following excavation to the maximum extent practicable, engineering and institutional controls (i.e., capping and an environmental covenant) may be a necessary element for the final remedy at the Site to address inaccessible soil contamination below the building. Additionally, engineering controls in the form of a vapor mitigation system may be required if soil impacts exceed screening levels for a vapor intrusion risk.

#### 4.1.2 Off-Property

The lateral extent of soil impacts exceeding Method A cleanup levels is shown on Figure 5 in the RI/FS. The potential for exceedances of gasoline and benzene extending off the property and into the right-of-way (ROW) to the north and east are acknowledged. However, excavation of SE 28th Street and 80th Avenue SE is not included in the scope of the interim cleanup action at this time because the cost is considered clearly disproportionate to the benefit in the context of MTCA. In other words, the cost of excavation and restoration of the ROW, given the number of sensitive utilities and potential disruption to traffic in the downtown core, is considered cost prohibitive and would not provide significant benefit to human health or the environment based on the current data and information provided in the RI/FS.

Pending the results of confirmation soil sampling at the property boundary following excavation, engineering and institutional controls (i.e., capping and an environmental covenant) may be a necessary element for the final remedy at the Site to address soil contamination in the ROW. An environmental covenant would need to be granted by the City of Mercer Island (the City). If the City will not accept the conditions for an environmental covenant, then an FS will be required to demonstrate the disproportionate cost analysis (DCA) in accordance with MTCA. If soil exceeding

Method A cleanup levels persists in the ROW, and it is not possible to negotiate an environmental convenant with the City, a no further action (NFA) will not be possible for the Site. However, a property-specific NFA may be an option pending the DCA.

#### 4.2 Groundwater

Given the nature and extent of contamination presented in Puget's RI/FS, depth to groundwater at the Site ranges between 3 and 12 feet bgs and monitoring wells area screened as deep as 25 feet bgs. The inferred lateral extents of groundwater impacts exceeding Method A cleanup levels is shown in plan view on Figures 9 and 10 of the RI/FS.

Given the depth to groundwater, the excavation for the interim cleanup action will require dewatering to reach the vertical depth of soil contamination. This will result in the removal and disposal of some petroleum-impacted groundwater; however, it is anticipated that a period of natural attenuation will still be necessary following removal of soil impacts on the property before groundwater will attain cleanup levels both on and off the property.

Additionally, if soil impacts remain in place on and/or off the property as discussed in Section 4.1, a lengthy period of attenuation can be expected for groundwater. In that event, engineering and institutional controls (i.e., capping and an environmental covenant) may be a necessary element for the final remedy at the Site to address groundwater. Additionally, engineering controls in the form of a vapor mitigation system may be required if groundwater impacts exceed screening levels for a vapor intrusion risk.

Similar to soil, an environmental covenant for off-property groundwater impacts would need to be granted by the City. If the City will not accept the conditions of an environmental covenant, then an FS will be required to demonstrate the DCA in accordance with MTCA. If groundwater exceeding Method A cleanup levels persists in the ROW, and it is not possible to negotiate an environmental covenant with the City, an NFA will not be possible for the Site. However, a property-specific NFA may be an option pending the DCA.

#### 4.3 Vapor

Soil gas and air were not evaluated as part of Puget's RI and remain as potential media of concern. The vapor exposure pathway remains to be evaluated following interim cleanup actions.

Pending the success of the interim cleanup action, a vapor assessment will be required if soil and groundwater impacts persist at the Site above Method A cleanup levels. Additionally, engineering controls in the form of a vapor mitigation system may be required as a necessary element of the final remedy at the Site if soil gas or indoor air impacts exceed screening levels for a vapor intrusion risk.

## 5 Interim Cleanup Action Plan

Given the current plans for redevelopment of the property, there is an opportunity to conduct an interim cleanup action to remove accessible soil and groundwater impacts from the property in conjunction with replacement of the underground storage tanks (USTs), pump islands, and canopy. This section presents the general approach and recommendations for the interim cleanup action to

meet the objectives of MTCA and comply with the regulation to the maximum extent practicable. The interim cleanup action will include for following elements:

- Decommissioning and removal of USTs, dispensers, piping, and ancillary equipment associated with the fueling system infrastructure, including demolition of the pump island canopy.
- Excavation and off-site disposal of petroleum impacted soil on the property to the maximum extent practicable.
- Groundwater management, dewatering, and disposal.
- Backfilling and site restoration.

These elements are described further below.

#### 5.1 Decommissioning and Removal of USTs and Ancillary Equipment

The USTs and associated belowground piping and dispensers will be decommissioned and removed during the source removal action in accordance with Ecology's current UST regulations (WAC 173-360) and other applicable state or local regulations. The Contractor will be a Certified UST Decommissioner and responsible for completing Ecology's 30-Day Notice and Permanent Closure Notice for USTs. A Certified Site Assessor will collect the required soil samples and complete Ecology's Site Check/Site Assessment Checklist at the time of decommissioning.

#### 5.2 Excavation and Off-Site Disposal of Petroleum Impacted Soil

The objective of the soil removal action is to remove the source of contamination in and around the UST basin, pump islands, and building to the maximum extent practicable.

#### 5.2.1 Soil Cleanup Levels for Interim Cleanup Action

The MTCA Method A cleanup levels described in Section 3 are applicable for this interim cleanup action. Every effort should be made to remove impacted soil on the property exceeding unrestricted cleanup levels. The COCs for the Site are identified in Section 2.

It is recognized that exceedances of the Method A cleanup level for COCs may remain in the ROW to the north and east of the property, pending performance and confirmation soil sampling results. MTCA implications for potential off-property soil impacts exceeding cleanup levels are discussed in Section 4.1 in the context of the final remedy for the Site.

#### 5.2.2 Excavation Extents and Shoring

Vertical shoring will be required along the north and east property boundaries to facilitate removal of the USTs and impacted soil up to the property line. Soil impacts to the south and west of the UST basin are delineated as shown on RI/FS Figure 5.

It is recognized that affected soil may extend under the east end of the building on the property and may require shoring to remove additional soil to the maximum extent practicable. If performance sampling indicates soil contamination extends a limited distance under the building, pin piles or micro piles are recommended to support the building and allow access for excavation.

The current shoring plan for construction is provided in Appendix B. To better meet the stated MTCA objectives of the interim cleanup action, it is recommended that the interior shoring alignment be eliminated and the shoring walls along the property lines be extended to the south and west to facilitate sloping of the excavation as necessary up to the south and west property boundary, pending performance soil sampling results.

It is also recommended that the vertical shoring along the north and east property boundaries be designed to facilitate excavation to a minimum depth of 16 feet for purposes of impacted soil removal around the UST basin. A vertical contingency of up to 2 feet is recommended to allow for additional soil removal at depth pending performance soil sampling results. The shoring design should also account for the depth of the planned UST replacement if deeper.

Detailed construction requirements for modifications to the shoring design to meet the interim cleanup action objectives, including permitting and shoring design, should be identified and performed by a structural engineer. The shoring design should also factor in considerations for dewatering of the excavation to achieve design excavation depths as discussed in Section 5.3.

The actual extent of the excavation, within the limitations of the shoring design, will be determined by collecting performance soil samples from the sidewalls and bottom of the excavation. Performance monitoring is described below in Section 5.2.3.

#### 5.2.3 Performance Monitoring

Performance monitoring of the soil removal action will include field screening and collection of soil samples for laboratory analysis during the excavation. Soil samples will be collected for the following reasons:

- To document COC concentrations in soils that are excavated.
- To characterize soil for disposal or reuse.
- To determine whether contaminant concentrations in soils that are left in place comply with applicable cleanup standards.

Soil sampling and analysis will be conducted in accordance with a project-specific Sampling and Analysis Plan (SAP). In general, soil samples will be collected using U.S. Environmental Protection Agency (EPA) Method 5035 sampling kits for gasoline and volatile compounds. Discrete grab samples will be submitted for analysis so that contaminant variability can be evaluated. Field screening techniques will generally be used to help ensure that a "worst-case" sample is collected for analysis. If a backhoe is used to collect the sample (e.g., when it is unsafe for the sampler to enter the excavation), care will be taken to ensure the backhoe bucket is clean of other soil before sampling. "Fresh" soils will be exposed just prior to sampling (to limit contaminant loss to volatilization), and the soil sample will be collected from the middle of the bucket, from soils that have not contacted the sides of the bucket. If sampling personnel can safely access the sampling location, a hand auger or shovel will be used to expose fresh soils just prior to sampling. Laboratory analyses of soil samples will include the following:

- DRO and ORO by Northwest Method NWTPH-Dx.
- GRO by Northwest Method NWTPH-Gx.

• BTEX and naphthalene by EPA Method 8260.

The overall scope of soil sampling and analysis activities will depend on field screening results, soil volumes, and treatment/disposal facility profiling requirements. In general, performance monitoring will include field screening and laboratory analysis of both excavation sidewall and bottom samples. The distance between sidewall samples will not exceed 20 feet, and closer sample spacing may be necessary. A minimum of one sample for approximately every 100 square feet of bottom area will be collected. njurg

Where soil sampling results indicate cleanup level exceedances, soil may be over excavated and resampled, if feasible, until sampling results are at or below the proposed cleanup levels. However, the excavation extent will be constrained as described in Section 5.2.2.

#### 5.2.4 Soil Management and Disposal

Based on the available soil characterization data, the excavated soils will be handled as:

- **Clean** (Category 1). Petroleum hydrocarbon contaminant concentrations are not detected and there is no odor, staining, or visible sheen. Generally, soils less than 3 feet bgs are expected to be clean.
- **Impacted** (Category 2). Petroleum hydrocarbon contaminants are detected below MTCA Method A cleanup levels.
- **Contaminated** (Categories 3 and 4). GRO and/or BTEX are detected above MTCA Method A cleanup levels. The soils between depths of 3 and 16 feet bgs are where the most contamination is expected to be located (i.e., around/below the USTs).

When evidence of petroleum hydrocarbon-contaminated soil is encountered (and no analytical data is available), visual and photoionization detector (PID) field screening techniques will be used to assess the extent of contamination and inform the segregation of impacted and contaminated soils. The segregation of soils will follow Ecology guidance (Ecology, 2016).

Given the limited space available on the Property, excavated soils that are known to be contaminated based on analytical data (or field-determined) will be direct loaded and hauled to a predetermined off-site treatment/disposal facility. It may be necessary to temporarily stockpile a limited amount of soil for final categorization and subsequent handling based on laboratory analytical results. Overburden soil screened as clean or impacted will be segregated and stockpiled for analytical testing and potential reuse. Stockpiling will include the following requirements:

- No material will be stockpiled in such a manner as to create surface water accumulation, impair access to adjacent sites of facilities, or be detrimental to the excavation in any way.
- Stockpiles will be constructed to isolate soils from the environment and encourage drainage of water from the soils. Stockpiles will be protected against erosion by wind and rain.
- Stockpiles will be underlain by plastic sheeting with a 10-millimeter minimum thickness, with adjacent sheeting sections overlapping a minimum of 3 feet.
- Berms will be constructed around each stockpile to a minimum height of 12 inches to prevent run-on of precipitation. Base liners of stockpiles will be bathtub construction to

collect excess water draining from the soil. Liquid accumulating in stockpiles will be collected and disposed of in accordance with applicable regulations at an approved treatment facility.

• Stockpiles will be covered with plastic sheeting of a 6-millimeter minimum thickness to prevent precipitation from entering the stockpile, and when not in use. The cover will be anchored to prevent it from being disturbed by wind.

#### 5.3 Groundwater Management, Dewatering, and Disposal

As noted in Section 4.2, depth to groundwater at the Site ranges between 3 and 12 feet bgs. Given the targeted depths of the excavation, the proposed interim cleanup action will require dewatering to reach the vertical depth of soil contamination.

Detailed construction requirements for dewatering to meet the interim cleanup action objectives, including permitting and design, should be identified and performed by a state-licensed hydrogeologist or professional engineer in coordination with the shoring design and construction contractor's planned means and methods for the excavation approach. Recommended performance criteria for excavation dewatering include:

- Dewater excavations as needed to maintain unsaturated conditions to facilitate soil excavation/handling/loading for transport, confirmation soil sampling in the excavation, and excavation backfilling.
- Collect and treat all water generated during dewatering to meet water quantity and quality requirements for discharge to sanitary sewer under an Individual Discharge Authorization from the City of Mercer Island and/or other appropriate agencies.
- Alternatively, pumped water may be conveyed to a water storage system. Water storage will be sized appropriately to contain the necessary volume of water with consideration for disposal frequency. Collected water will be disposed of in accordance with applicable regulations at an approved treatment facility.

#### 5.4 Backfilling and Site Restoration

Backfilling and site restoration activities are expected to be specified in the design for the UST system replacement. We recommend securing the appropriate permits and preparing a completed set of plans and specifications, stamped by a licensed professional engineer in the State of Washington, for replacement of the UST system. The UST system should be designed to meet or exceed current UST regulations (WAC 173-360). The existing dispensers, and automated tank monitoring system and associated sensors, may be reused unless prohibited by WAC 173-360.

As discussed in Section 5.2.2, it is recommended that the shoring system be designed to meet the objectives of the interim cleanup action action as well as the UST system replacement. Detailed construction requirements to accommodate UST replacement, including any additional permitting and shoring design beyond the scope of the interim cleanup action, should be identified and performed in conjunction with a structural engineer.

# 6 Conclusions and Recommendations

The purpose of this ICAP is to define the objectives of the cleanup activities that will be performed in conjunction with replacement of the gas station infrastructure on the property, identify additional

engineering needs to meet MTCA objectives, and make recommendations for the current planning efforts where appropriate to meet those objectives.

Based on the applicable cleanup levels and areas requiring remediation at the Site, the following engineering needs and planning efforts are recommended to provide a higher level of assurance that the interim cleanup action will meet MTCA requirements and result in closure:

- Recognizing there are multiple potential paths for achieving closure at this Site or property, and they are dependent on the outcome of the interim cleanup action. Future requirements may include vapor assessment and/or mitigation, capping areas of contamination, environmental covenants for potential residual impacts both on- and/or off-property, and an additional feasibility study to support selection of a final remedy.
- Engaging the City to review the potential outcomes of the interim cleanup action as discussed in Section 4 with respect to the potential need for engineering and institutional controls to address the potential for off-property contamination and closing the Site.
- Modifying the shoring approach as recommended in Section 5.2.2 to provide greater flexibility for achieving applicable cleanup standards during excavation.
- Preparing a SAP and soil management plan for performance sampling and management of soil during the excavation as recommended in Section 5.2.3 and 5.2.4.
- Preparing a dewatering plan as recommended in Section 5.3 to maximize the depth of excavation, within the limitations of the shoring design, and remove soil impacts to the maximum extent practicable.
- Preparing plans for replacement of the fueling system infrastructure and site restoration activities as recommended in Section 5.4.

To the extent these recommendations trigger additional permitting and/or design requirements with the City, the efforts related to meeting those requirements should be considered reasonable and necessary for the cleanup of the Site. It is recommended that the insurance policy holder engage the insurance company for review and a determination of coverage for those activities as necessary.

#### Limitations

Work for this project was performed for Sun Pacific Energy (Client), and this memorandum was prepared in accordance with generally accepted professional practices for the nature and conditions of work completed in the same or similar localities, at the time the work was performed. This memorandum does not represent a legal opinion. No other warranty, expressed or implied, is made.

All reports prepared by Aspect Consulting for the Client apply only to the services described in the Agreement(s) with the Client. Any use or reuse by any party other than the Client is at the sole risk of that party, and without liability to Aspect Consulting. Aspect Consulting's original files/reports shall govern in the event of any dispute regarding the content of electronic documents furnished to others.

Please refer to Appendix C titled "Report Limitations and Guidelines for Use" for additional information governing the use of this report.

# **MEMORANDUM**

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Attachments: Appendix A – Puget Environmental RI/FS Appendix B – Allstructure Engineering Shoring Plan Appendix C – Report Limitations and Guidelines for Use

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# **APPENDIX A**

Puget Environmental RI/FS

# PUGET ENVIRONMENTAL P.L.L.C.

January 22, 2020

Mr. George Stokes Mercer Island Shell Service Station 7833 Southeast 28th Street Mercer Island, Washington

### Subject: Remedial Investigation and Feasibility Study Report Mercer Island Shell Service Station (Former BP) 7833 Southeast 28th Street Mercer Island, Washington

Dear Mr. Stokes:

In accordance with your request, Puget Environmental, PLLC (Puget) has prepared this remedial investigation and feasibility study report for the Mercer Island Shell Service Station located at 7833 Southeast 28th Street, in Mercer Island, Washington. The report has been prepared to summarize previous investigation results and conclusions and provide recommendations for final cleanup and site closure under the Washington State Model Toxics Control Act (MTCA) Cleanup Regulation, Chapter 173-340 WAC.

#### SITE DESCRIPTION

The site consists of an approximately 0.30 acre parcel located approximately 84 feet above mean seal level near the northern shore of Mercer Island. Lake Washington is present approximately 1,870 feet to the northwest. Luther Burbank Park is present approximately 1,470 feet to the north and west. The area around the site is relatively level. The site location is shown of Figure 1.

The site is bounded by Southeast 28th Street to the north and 80th Avenue Southeast to the east. A professional building is present on adjacent property to the south. A grocery store is present on the adjacent property to the west. Properties in remaining directions are occupied by a mix of commercial and professional facilities. Residences are present approximately 165 feet to the north and west. The site and areas of nearby property use are shown on Figure 2.

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Records indicate the site has been operated as an automobile service station since the 1950s. The site is currently occupied by an active gasoline service station with four dispensers and three underground storage tanks (USTs) containing unleaded gasoline. A used oil UST was reportedly present on site at one time and removed prior to 1995. Washington State Department of Ecology (Ecology) records indicate the current USTs were installed in 1985 and 1986. A convenience store and auto repair shop are also present at the site. A total of 24 groundwater monitoring wells and 2 vapor extraction wells are present on and off site. Monitoring well locations and select site features are shown on Figure 3.

#### **REMEDIAL INVESTIGATION**

Following is a summary of historic and recent investigations and results based on review of previous consultants' reports as provided by the property owner as well as Puget's investigation results. A list of the references reviewed is attached.

#### Initial Investigation and Remediation System Operation

Petroleum hydrocarbon-impacted soil and groundwater at concentrations exceeding applicable cleanup levels were first identified beneath the site during a Phase II environmental site assessment conducted by AGRA Earth & Environmental, Inc. in December 1995.

Following discovery of the impacts, a combined soil-vapor extraction (SVE) and groundwater extraction (GWE) remediation system was reportedly installed to treat the impacts. The remediation system consisted of 3 extraction tranches that treated and discharged groundwater into the sanitary sewer system.

In December 2000, Camp Dresser & McKee (CDM) modified the remediation system and installed a 200-gallon aeration tank and modified the conveyance piping to eliminate discharge to storm sewer and into a new infiltration trench. SVE activities were discontinued at this time.

In January 2006, Delta Environmental Consultants Inc. (Delta) further modified the existing remediation system to utilize high vacuum dual phase extraction (HVDPE). Liquids and vapors were extracted from two of four on-site wells.

In June 2010, the remediation system operation was discontinued. The vapor and groundwater extraction equipment was subsequently dismantled and removed.

#### Additional Investigation

Following remediation system operation, additional investigations were subsequently conducted to further evaluate groundwater conditions and the extent of remaining impacted soil. Groundwater monitoring and sampling activities were reportedly conducted by Antea Group in 2012. Environmental Partners Inc. (EPI) subsequently advanced 12 soil borings (DP-1 through DP-12) and drilled and installed 7 additional monitoring wells (MW-5, MW-6, MW-7, MW-10 MW-11, MW12S and MW12D) and 2 soil vapor extraction wells (SVE-1 and SVE-2) in 2012 and 2013. Soil and groundwater analytical results are presented in EPI reports from February 2013 through January 2015.

Between 2015 and 2017, Puget conducted additional investigation to further evaluate the migration and extent of impacted soil and groundwater. A total of 8 additional monitoring wells (MW-13 through MW-20 were installed on and off site.

Following review by the Washington State Pollution Liability Insurance Agency (PLIA) 4 additional monitoring wells (MW-21 through MW-24) were installed to further evaluate shallow subsurface conditions. Results of the most recent monitoring and sampling events are presented in reports prepared by Puget dated February 8, 2019 and September 17, 2019.

#### GEOLOGIC AND HYDROGEOLOGIC SETTING

Geologic records indicate the site is underlain by Quaternary Vashon till deposits consisting of a compact diamict of silt, sand and subrounded to well-rounded gravel, glacially transported and deposited under ice.

Results of drilling and soil sampling conducted by CDM, Delta, EPI and Puget indicate the site is generally underlain by damp to wet, silty clay to clayey silt to approximately 15 to 20 feet below ground surface (bgs) where it is underlain by saturated fine-grained sand to the maximum depth explored of approximately 25 feet bgs. Groundwater in the underlying sandy zone appears to be partially confined by the overlying clay and silt.

Review of Ecology well log records indicates groundwater approximately 115 and 116.5 feet bgs in two water supply wells located approximately 1,300 feet southeast of the site.

Review of historic groundwater monitoring and sampling results indicate groundwater approximately 3 to 11 feet bgs beneath the site with a variable gradient generally directed toward the northwest at a magnitude of approximately 0.01. A groundwater contour map with results of the most recent sampling event conducted in August 2019 is shown on Figure 4 along with a rose diagram depicting historic groundwater gradient directions.

### **CONTAMINANTS OF CONCERN**

The history of operations at the property and analytical results indicate the following contaminants of concern (COCs) for both soil and groundwater beneath the site:

- Total petroleum hydrocarbons as gasoline (TPH-G) and as diesel (TPH-D)
- Benzene, toluene, ethylbenzene and total xylenes (BTEX)

### POINTS OF COMPLIANCE

- The point of compliance for soil based on protection of groundwater is all soil throughout the site.
- The point of compliance for groundwater is all groundwater from the uppermost level of the saturated zone extending vertically to the lowest depth that is affected by any of the COCs at the site.
- The point of compliance for air is all air throughout the site.

## NATURE AND EXTENT OF CONTAMINATION

#### Soil

Results of previous and recent investigations indicates petroleum hydrocarbon-impacted soil at concentrations exceeding the MTCA Method A cleanup levels is present approximately 3 to 16 feet bgs near and between the USTs and dispenser islands. The estimated extent of impacted soil is shown on Figure 5. Cross-sections through the impacted areas are shown in Figures 6 through 8. Based on results of all known investigations to date, it appears up to approximately 1,500 cubic yards of soil may have been impacted.

#### Groundwater

Results of historical groundwater sampling activities conducted between 1995 and 2019 indicate groundwater samples collected from MW-1, MW-2, MW-4, MW-5, MW-7, MW-10, MW-11, MW-12S, MW-12D, MW-19, MW-21, SVE-1 and SVE-2 have historically contained TPH-G, TPH-D and/or BTEX concentrations exceeding the MTCA Method A cleanup levels. Sampling results do not reveal indications of off-site groundwater impacts and there are no indications that subsurface utilities have provided preferential pathways for contaminant migration. Based on results of the most recent groundwater monitoring and sampling events conducted by Puget in February and August 2019, it appears impacted groundwater is limited to the area immediately adjacent to the USTs. The estimated extent of gasoline- and benzene-impacted groundwater from the February 2019 sampling event is shown on Figures 9 and 10.

Historical groundwater results are shown on Tables 1 and 2.

#### CONCEPTUAL SITE MODEL

Based on investigation results, a Conceptual Site Model has been prepared in accordance with WAC 173-340-708(3)(e) to evaluate potential exposure pathways. Results of the Conceptual Site Model Evaluation indicate the following potential complete exposure pathways:

#### <u>For Soil –</u>

• Direct contact and ingestion by construction workers and terrestrial biota

#### For Groundwater –

• Direct contact and ingestion by construction workers and terrestrial biota

#### For Vapor –

• Inhalation by commercial and construction workers

#### TERRESTRIAL ECOLOGICAL EVALUATION

In accordance with WAC 173-340-7490, a Terrestrial Ecological Evaluation (TEE) has been conducted to determine cleanup levels that are applicable to the site for the protection of potential terrestrial receptors. Based on results, Puget proposes using the concentrations listed in Table 749-3 as cleanup levels, pending agency review and approval.

#### CONCLUSIONS

#### Soil

Review of drilling and sampling data indicate the site is generally underlain by damp to wet silty clay to clayey silt from the surface to approximately 15 to 20 feet bgs where it is underlain by saturated fine-grained sand to the maximum depth explored of approximately 25 feet bgs. Based on review of historic and recent investigation results, it appears up to approximately 1,500 cubic yards of petroleum hydrocarbon-impacted soil remains present approximately 3 to 16 feet bgs near and between the USTs and dispenser islands (Figures 5 through 7).

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#### Groundwater

Review of historic groundwater monitoring and sampling results indicates groundwater approximately 3 to 11 feet bgs beneath the site with a variable gradient generally directed toward the northwest at a magnitude of approximately 0.01 (Table 1 and Figure 4). Groundwater in the underlying sandy zone appears to be partially confined by the overlying clay and silt.

Historic and recent laboratory results indicate groundwater immediately adjacent to the USTs is impacted with TPH-G and benzene at concentrations exceeding the MTCA Method A cleanup level (Figures 9 and 10).

#### FEASIBILITY STUDY

#### **Soil and Groundwater Conditions**

Results of previous investigations indicate approximately 1,500 cubic yards of impacted soil is present near and between the dispensers and USTs. Impacted soil consists primarily of silty clay and clayey silt with relatively low hydraulic conductivity in the range of approximately 10<sup>-8</sup> to 10<sup>-9</sup> centimeters per second.

Based on a review of historic remediation system operations and the low hydraulic conductivity properties of impacted soil, it appears prior in situ remediation techniques have removed contaminants from subsurface to the maximum extent practicable based on soil and groundwater conditions. Therefore, in order to complete cleanup within a reasonable timeframe, it appears more aggressive remediation will be needed.

#### **Proposed Cleanup**

<u>Soil</u>

Based on conditions, Puget has conducted a limited feasibility study to evaluate potential remedial options based on the soil conditions and the depth and location of contaminants. Based on technical considerations and results of disproportionate cost analysis conducted under WAC 173-340-360 (3)(e) Puget recommends excavation and removal of impacted soil near and between the USTs and dispensers as the preferred remedial option.

Based on over 30 years of operation and the documented presence of subsurface impacts, Puget recommends removal and replacement of the existing USTs and piping as part of the proposed cleanup of the site.

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Once the existing USTs and piping have been removed, we recommend excavation and removal of remaining impacted soil near and between the dispenser islands and USTs.

#### **Groundwater**

Based on the depth to groundwater and the soil type and depth to impact, dewatering and removal of impacted groundwater will likely be needed during excavation and removal of impacted soil to be conducted in conjunction with UST replacement. Based on the relatively limited extent of impact, soil excavation along with dewatering and removal of impacted groundwater during will likely remove the majority of remaining contaminants. A brief period of natural attenuation monitoring may be needed to document and confirm soil and groundwater cleanup once excavation and tank replacement is completed.

Estimated costs for the proposed cleanup are shown on Table 3.

#### LIMITATIONS

The scope of work for this investigation was conducted in a manner that is consistent with the level of care and skill ordinarily exercised by other members of the profession practicing in the same locality and under similar conditions as of the date the services were provided. Results of our evaluation including conclusions, opinions and recommendations are based on a limited number of observations and data. Data from other areas may be different. Puget makes no representation, guarantee, or warranty, express or implied, regarding the services, communication, report, opinion, or instrument of service provided.

Puget provides various levels of service to meet the needs of varying clients. Evaluation of geologic and environmental conditions requires judgment leading to conclusions and recommendations that are generally based on incomplete knowledge of subsurface conditions due to the limitations of data from field studies. Although risk cannot be eliminated, more detailed and extensive studies yield more information which may help understand and manage the level of risk.

The work was conducted based on the scope and budget requirements, and site information provided by our client.



We appreciate the opportunity to provide service. Please do not hesitate to contact either of the undersigned if you have any questions.

Sincerely,

Puget Environmental, PLLC

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John P. Meyer Project Manager

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John K. Meyer, L.HG. Principal Hydrogeologist

Attachments

References Reviewed Figures Tables Boring Logs and Well Construction Diagrams

#### **REFERENCES REVIEWED**

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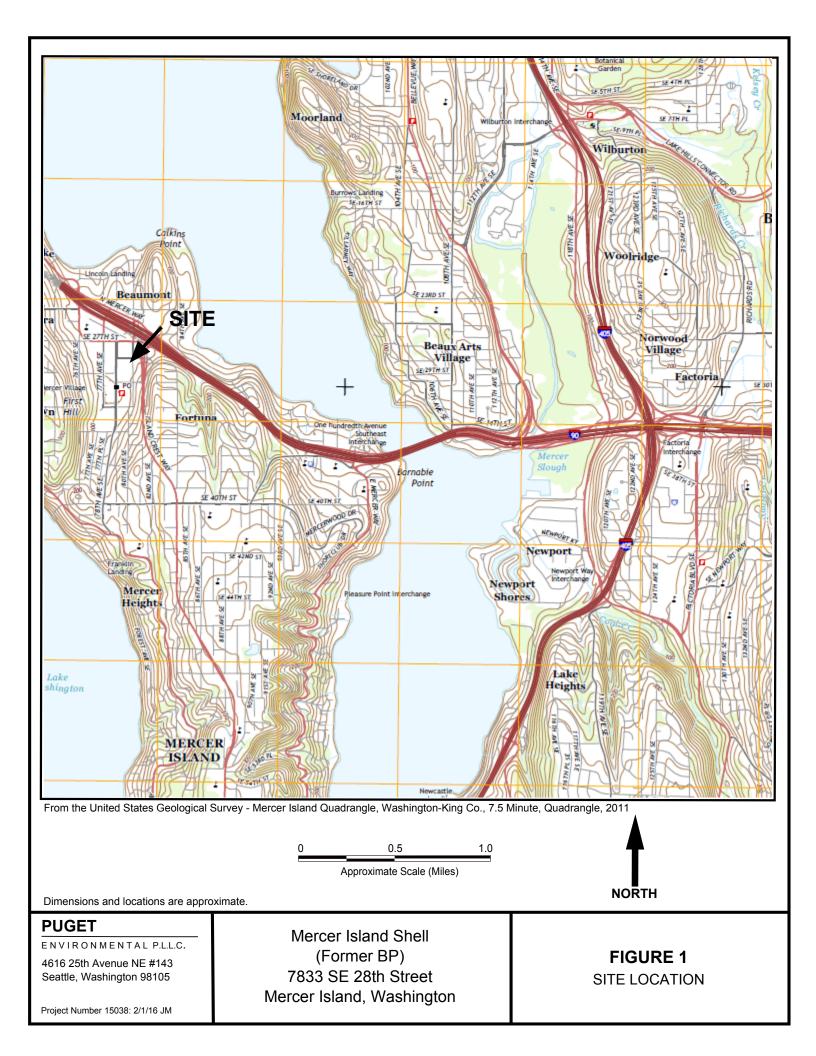
Puget Environmental P.L.L.C., Monitoring Well Installation and Sampling, Mercer Island Shell (Formerly BP), April 17, 2017

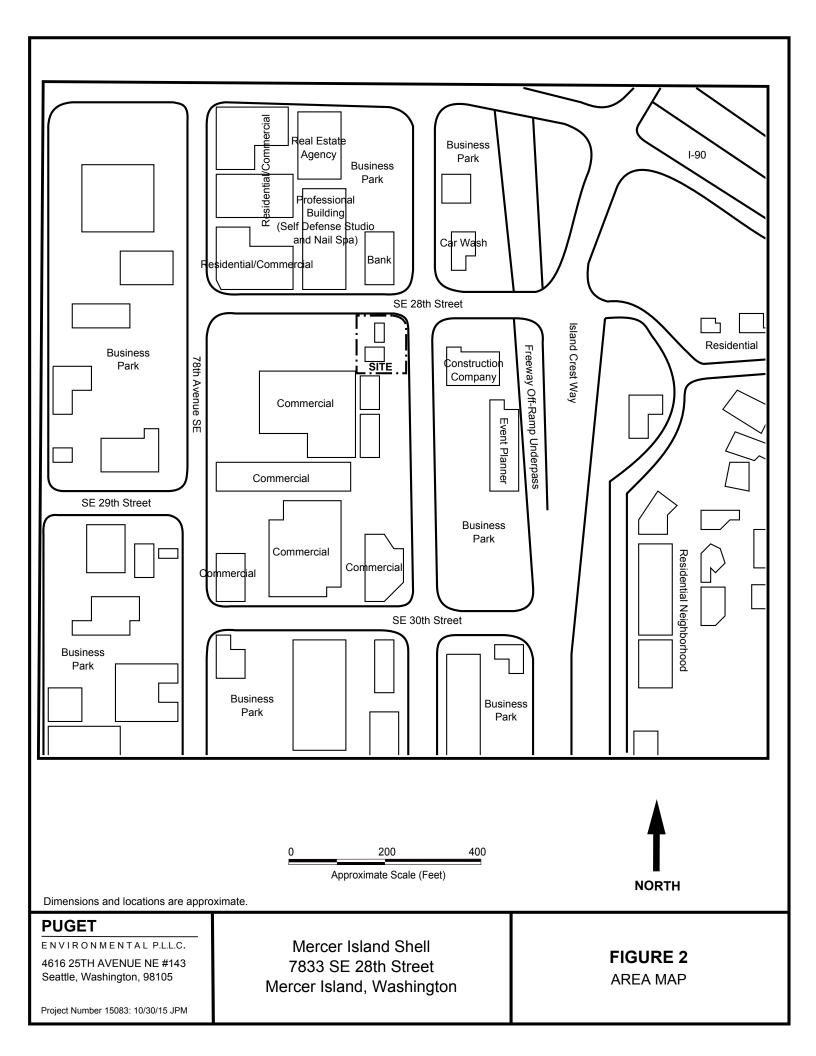
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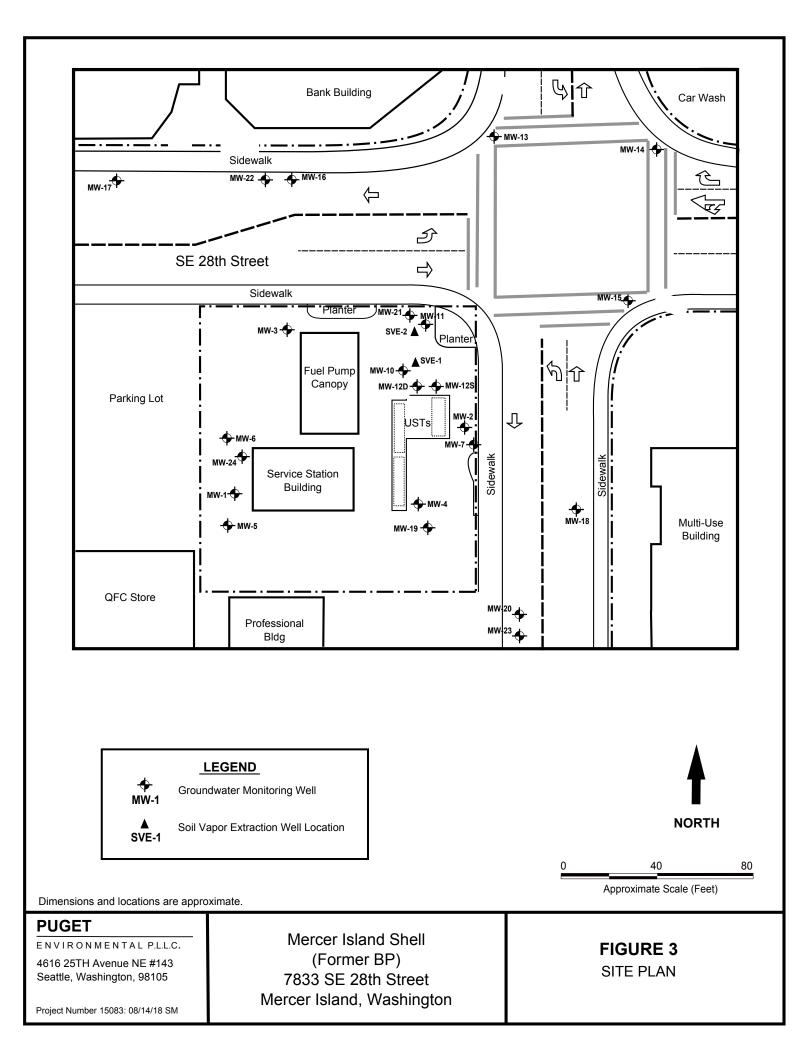
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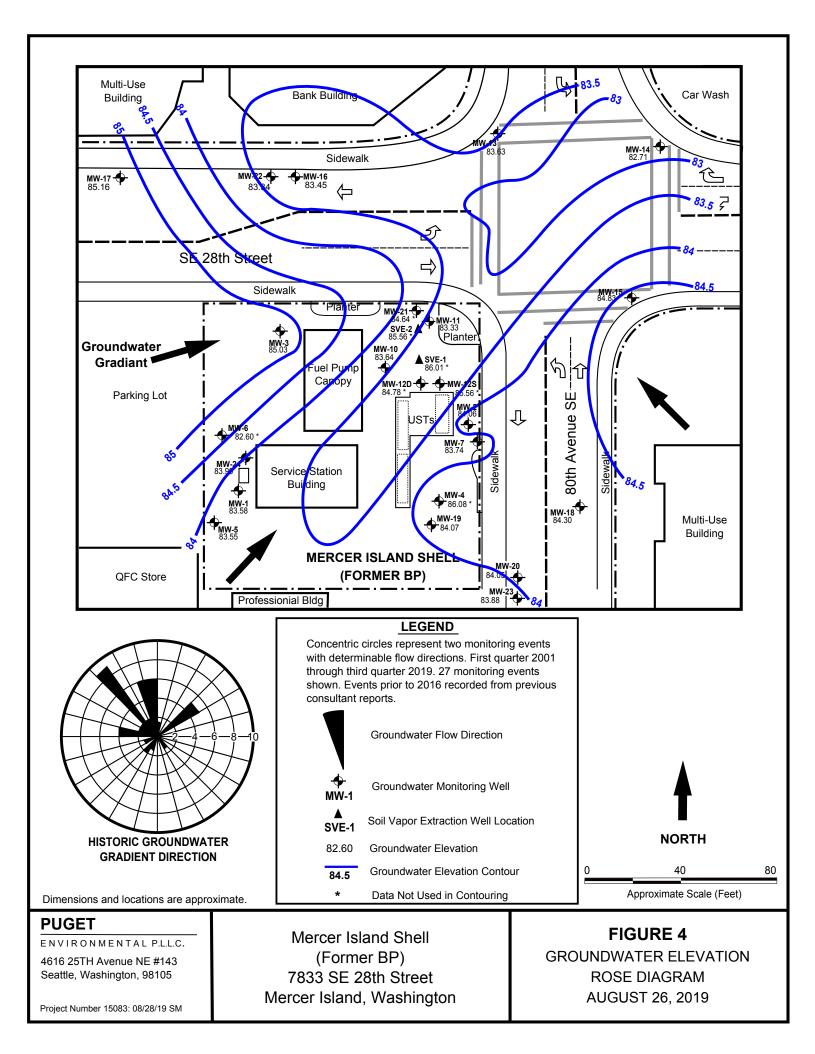
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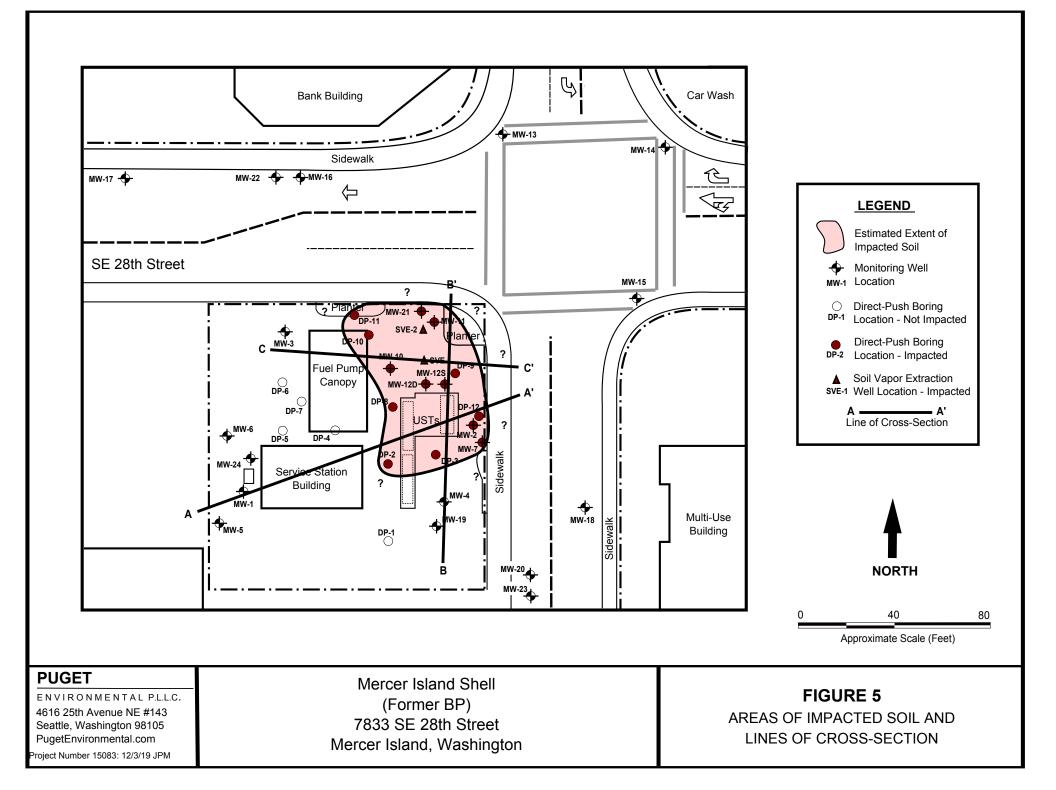
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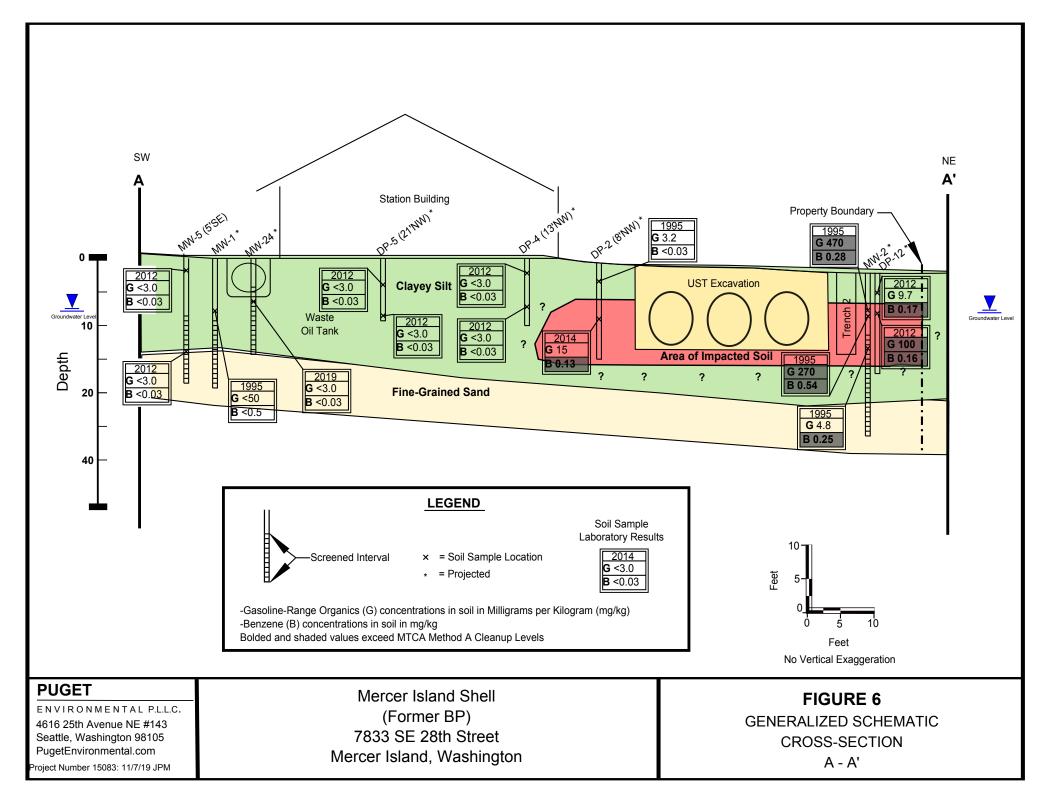


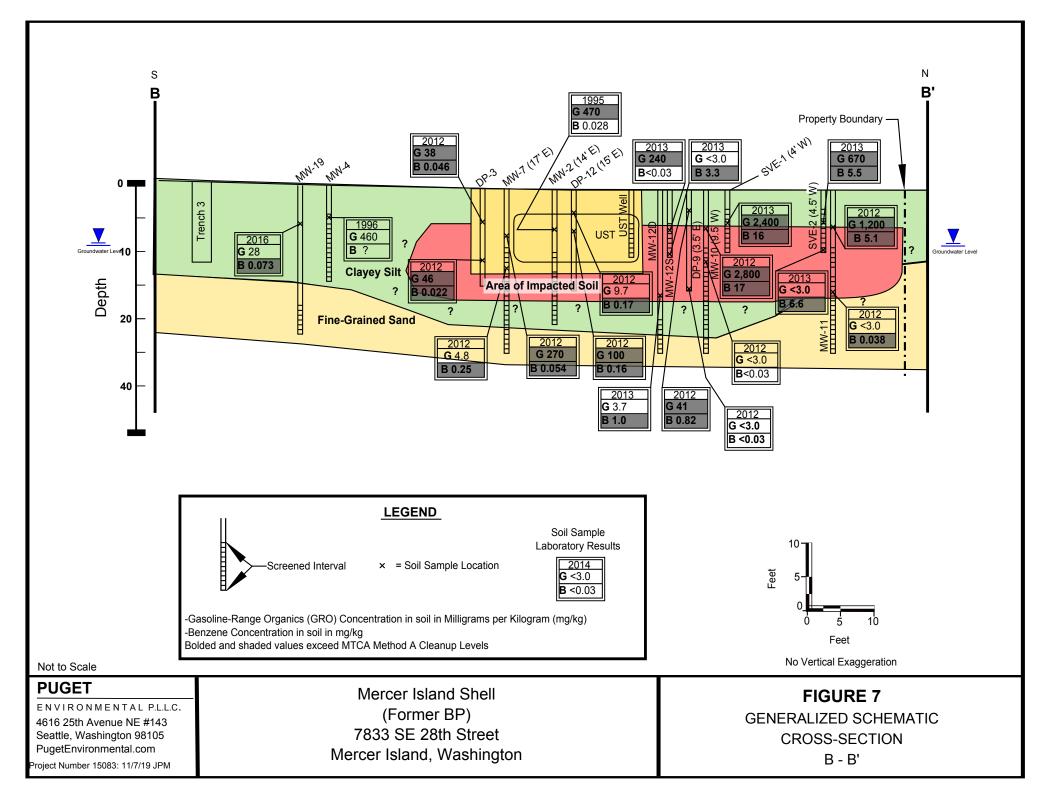


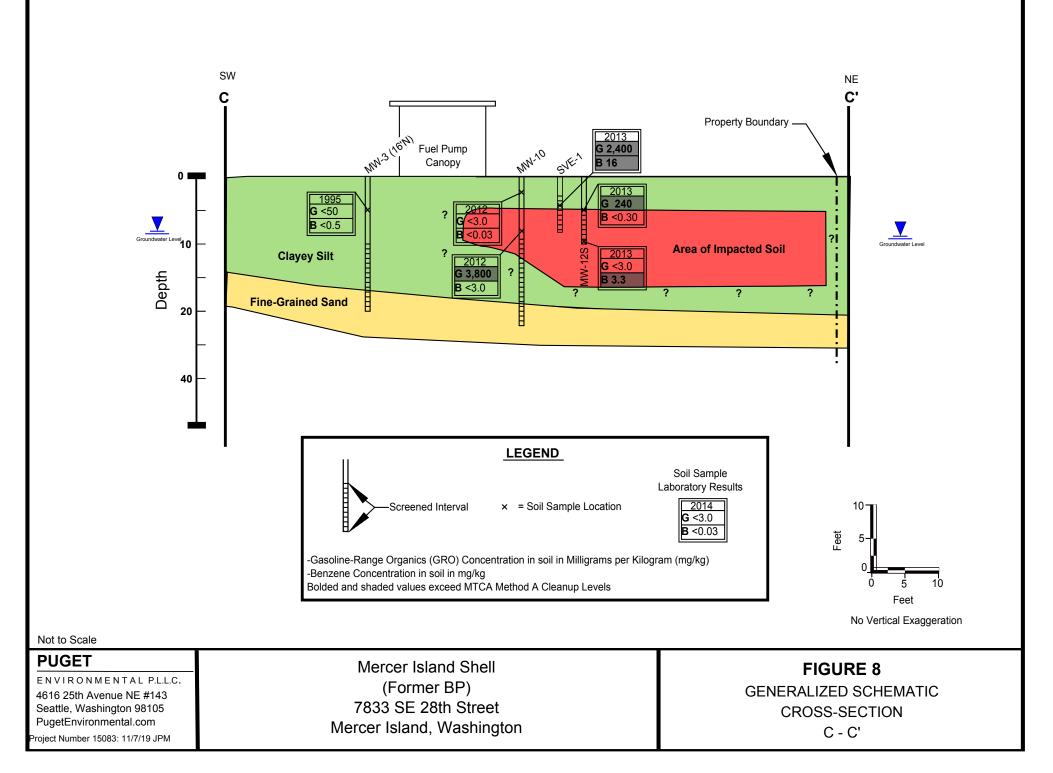


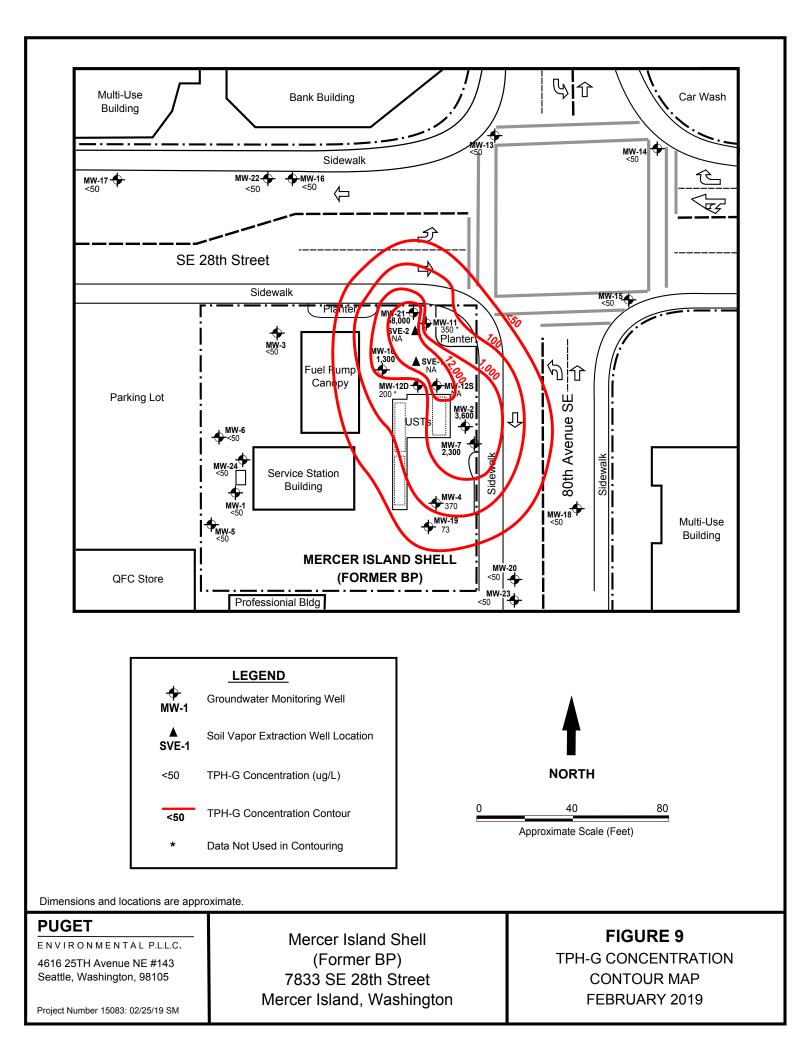


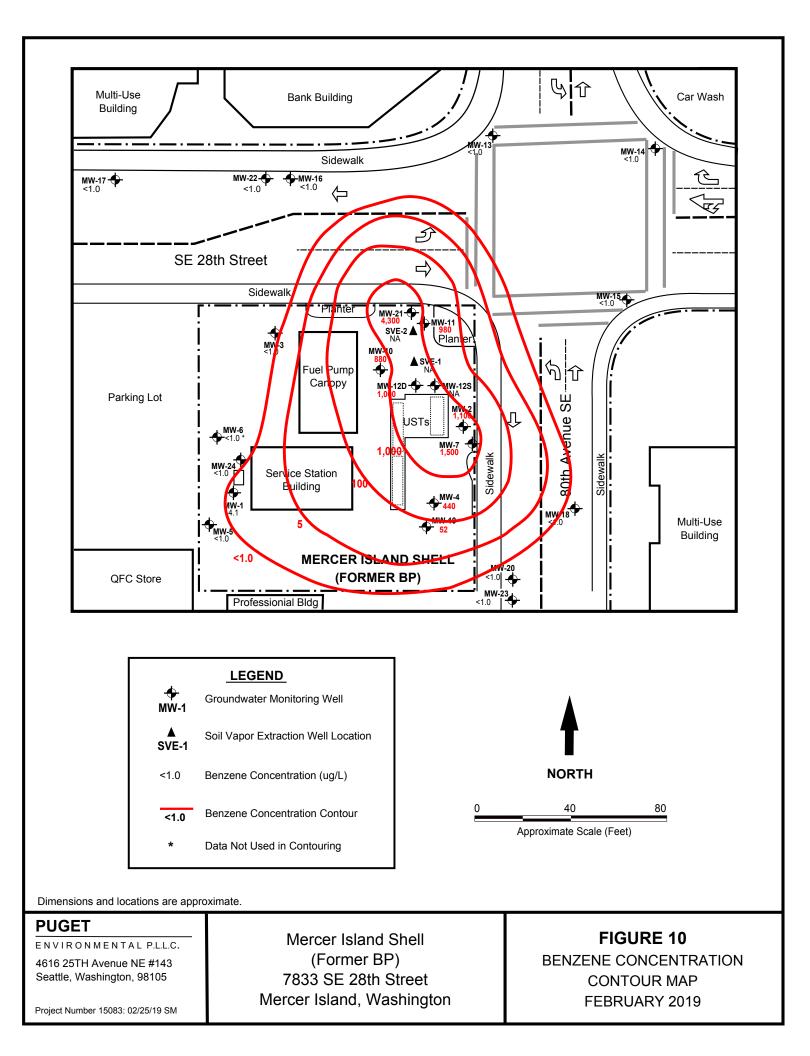












Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	трн-о	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-1	12/29/95			ND			ND	ND	ND	ND	ND	
94.07	04/19/96			ND			ND	ND	ND	ND		
	05/16/97	7.39	86.68	ND			ND	ND	ND	ND		
	04/06/00	7.76	86.31	ND			ND	ND	ND	ND		
	07/20/00	8.91	85.16	ND			ND	ND	ND	ND		
	11/17/00	9.09	84.98	ND			ND	ND	ND	ND		
	02/27/01	8.05	86.02	ND			ND	ND	ND	ND		
	06/04/01	8.14	85.93	ND			ND	ND	ND	ND		
	09/27/01	8.19	85.88	ND			ND	ND	ND	ND		
	12/28/01	8.30	85.77	ND			ND	ND	ND	ND		
	03/13/02	7.29	86.78	ND			ND	ND	ND	ND		
	06/14/02	7.81	86.26	ND			ND	ND	ND	ND		
	09/26/02	9.19	84.88	ND			ND	ND	ND	ND		
	12/05/02	9.10	84.97	ND			ND	ND	ND	ND		
	03/06/03	8.15	85.92	200			8	ND	2	8		
	06/04/03	8.21	85.86	ND			ND	ND	ND	ND		
	09/10/03	8.61	85.46	ND			ND	ND	ND	ND		
	11/25/03	7.59	86.48	ND			ND	ND	ND	ND		
	02/26/04	7.70	86.37	NS			NS	NS	NS	NS		
	03/11/04	7.39	86.68	ND			ND	ND	ND	ND		
	06/16/05	9.15	84.92	ND			ND	ND	ND	ND		
	09/15/05	9.15	84.92	ND			ND	ND	ND	ND		
	12/15/05	9.42	84.65	ND			ND	ND	ND	ND		
	03/16/06	8.88	85.19	ND			ND	ND	ND	ND		
	06/12/06	9.37	84.70	ND			ND	ND	ND	ND		
	09/20/06	9.85	84.22	ND			ND	ND	ND	ND		
	12/14/06	8.47	85.60	ND			ND	ND	ND	ND		
	03/16/07	12.10	81.97	ND			ND	ND	ND	ND		
	06/21/07	9.95	84.12	ND			ND	ND	ND	ND		
	09/25/07	10.28	83.79	ND			ND	ND	ND	ND		
	12/21/07	9.16	84.91	ND			ND	ND	ND	ND		
	03/17/08	9.39	84.68	ND			ND	ND	ND	ND		
	06/16/08	9.84	84.23	ND			ND	ND	ND	ND		
	10/02/08	10.11	83.96	ND			ND	ND	ND	ND		
	12/04/08	9.77	84.30	ND			ND	ND	ND	ND		
	03/02/09	9.21	84.86	ND			ND	ND	ND	ND		
	06/11/09	9.85	84.22	<50			<1	<1	<1	<3		

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-1	12/07/09	9.36	84.71	<50			<1.0	<1.0	<1.0	<3.0		
(Continued)	03/02/10	9.54	84.53	<50			<1.0	<1.0	<1.0	<3.0		
	09/26/11	10.37	83.70	54			9	<1.0	1.0	<3.0	<0.030	
	12/14/11	10.17	83.90	120			47	1.7	6.2	7.0		
	03/15/12	9.69	84.38	150			71	1.2	5.6	<3.0		
	09/24/12	10.83	83.24	<50			3	<1.0	1.2	<3.0	<1.0	
	12/06/02	8.65	85.42	92			31	2.9	4.7	5	<1.0	
	03/07/13	8.76	85.31	86			61	1.2	4.1	<3.0	<1.0	
	10/01/13	9.50	84.57	<50			<1.0	<1.0	<1.0	<3.0		
	07/06/15	10.14	83.93	<50			4	<1.0	<1.0	<3.0		
	01/13/16	9.11	84.96									
	06/15/16	9.81	84.26	<50	<130	<250	5	<1.0	<1.0	<3.0	<1.0	<1.0
	09/21/16	9.11	84.96									
	02/15/17	8.25	85.82	66	<130	<250	16	<1.0	2.3	<3.0	<1.0	<1.0
	10/24/17	10.09	83.98	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	8.99	85.08	<50	<130	<250	10	<1.0	2.7	<3.0		
	04/04/18	8.75	85.32	<50	<130	<250	5	<1.0	<1.0	<3.0		
	07/24/18	10.34	83.75									
	02/18/19	8.96	85.11	<50	160	<250	4.1	<1.0	<1.0	<3.0	<1.0	<1.0
	08/28/19	10.49	83.58	<50	130	<250	<1.0	<1.0	<1.0	<3.0		
MW-2	12/29/95			15,000			6,300	140	340	34	ND	
90.97	04/19/96			10,000			1,500	400	1,700	1,500		
	05/16/97	5.47	85.50	8,700			11,400	116	1,410	1,240		
	04/06/00	5.49	85.48	4,700			4,400	ND	990	110		
	07/20/00	7.37	83.60	3,800			3,100	ND	760	100		
	11/17/00	7.23	83.74	2,500			4,000	10	290	90		
	02/27/01	6.47	84.50	2,800			2,300	20	89	190		
	06/04/01	5.24	85.73	3,400			2,400	240	140	310		
	09/27/01	7.08	83.89	2,400			2,900	10	94	79		
	12/28/01	7.43	83.54	3,800			2,000	38	100	250		
	03/13/02	7.93	83.04	3,800			2,700	36	780	460		
	06/14/02	5.70	85.27	1,500			2,600	11	30	87		
	09/26/02	6.18	84.79	2,200			2,700	7	55	50		
	12/05/02	5.64	85.33	3,000			1,500	14	130	190		
	03/06/03	7.53	83.44	2,300			2,000	6	36	120		
	06/04/03	5.45	85.52	3,200			1,200	40	140	230		
	06/18/03	NM		4,650			2,010	16	12	75		
	07/01/03	NM		6,400			490	110	150	820		
	07/02/03	NM		1,200			1,600	13	5	49		
	09/10/03	6.64	84.32	1,400			2,000	6	7	19		

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-2	11/25/03	4.98	85.99	35,000			8,900	9,400	670	2,700		
(Continued)	02/26/04	4.52	86.45	24,000			1,700	2,700	410	2,600		
	03/11/04	4.60	86.39	37,000			2,100	3,600	1,100	5,200		
	06/16/05	5.32	85.65	2,700			1,700	24	50	120		
	09/15/05	6.38	84.59	5,200			640	110	120	420		
	12/15/05	6.03	84.94	2,800			1,200	22	81	130		
	03/16/06	3.58	87.39	50,000			3,500	400	1,400	5,800		
	06/12/06	5.49	85.48	7,600			1,200	500	200	950		
	09/20/06	6.43	84.54	3,500			1,900	13	34	330		
	12/14/06	4.71	86.26	3,100			880	ND	31	300		
	03/16/07	8.05	82.92	3,500			270	ND	42	270		
	06/21/07	9.60	81.37	920			1,600	ND	24	89		
	09/25/07	7.31	83.66	3,200			460	110	12	280		
	12/21/07	4.78	86.19	1,900			380	ND	10	53		
	03/17/08	5.61	85.36	1,700			1,100	5	18	22		
	06/16/08	7.20	83.77	390			1,300	2	5	20		
	10/02/08	7.40	83.57	1,300			490	3	8	40		
	12/04/08	6.28	84.69	1,200			890	3	11	16		
	03/02/09	5.85	85.12	1,800			530	4	26	60		
	06/11/09	6.74	84.23	840			580	2	14	12		
	09/21/09	7.69	83.28	910			120	2.1	26	110		
	12/07/09	6.14	84.83	1,100			140	3.1	17	97		
	03/02/10	5.85	85.12	840			200	1.5	22	31		
	09/26/11	1.39	83.58	1,500			740	20	35	40	7.6	
	12/14/11	6.60	84.37	1,800			620	9.9	41	41		
	03/15/12	8.30	82.67	2,600			760	14	44	39		
	09/25/12	7.35	83.62	2,000			900	17	14	23	<1.0	
	12/06/12	6.05	84.92	1,600			570	7.3	17	20	<1.0	
	03/08/13	5.10	85.87	2,500			840	16	50	52	<1.0	
	10/02/13	6.04	84.93	2,100			540	6.9	20	30		
	07/06/15	6.65	84.32	1,700			540	20	14	<30		
	01/13/16	5.10	85.87									
	06/16/16	5.97	85.00	2,000	900	<250	940	72	63	46	<1.0	<1.0
	09/21/16	5.10	85.87									
	02/15/17	4.62	86.35	4,300	880	<250	690	28	55	120	<1.0	<1.0
	10/24/17	6.52	84.45	3,300	860	340	720	19	18	43	<1.0	<1.0
	01/17/18	4.91	86.06									
	04/06/18	5.11	85.86	3,700	1,300	330	1,000	140	90	73		
	07/24/18	6.75	84.22									
	02/18/19	4.93	86.04	3,600	1,600	400	1,100	93	79	110	<1.0	<1.0
	08/27/19	6.91	84.06	NS	NS	NS	NS	NS	NS	NS	NS	NS

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-3	04/19/96			ND			ND	ND	ND	ND		
92.74	05/16/97	4.56	88.18	ND			ND	ND	ND	ND		
	04/06/00	4.88	87.86	ND			ND	ND	ND	ND		
	07/20/00	10.90	81.84	ND			ND	ND	ND	ND		
	11/17/00	11.13	81.61	ND			ND	ND	ND	ND		
	02/27/01	11.17	81.57	ND			ND	ND	ND	ND		
	06/04/01	11.05	81.69	ND			ND	ND	ND	ND		
	09/27/01	12.29	80.45	ND			ND	ND	ND	ND		
	12/28/01	11.12	81.62	ND			ND	ND	ND	ND		
	03/13/02	11.05	81.69	ND			ND	ND	ND	ND		
	06/14/02	11.17	81.57	ND			ND	ND	ND	ND		
	09/26/02	10.74	82.00	ND			ND	ND	ND	ND		
	03/06/03	11.02	81.72	ND			ND	ND	ND	ND		
	06/04/03	7.27	85.47	ND			ND	ND	ND	ND		
	09/10/03	5.72	87.02	ND			ND	ND	ND	ND		
	11/25/03	4.66	88.08	ND			ND	ND	ND	ND		
	02/26/04	4.55	88.19	ND			ND	ND	ND	ND		
	03/11/04	4.48	88.26	ND			ND	ND	ND	ND		
	06/16/05	5.45	87.29	ND			ND	ND	ND	ND		
	09/15/05	6.51	86.23	ND			ND	ND	ND	ND		
	12/15/05	6.01	86.73	ND			ND	ND	ND	ND		
	03/16/06	4.98	87.76	ND			ND	ND	ND	ND		
	06/12/06	7.50	85.24	ND			ND	ND	ND	ND		
	09/20/06	9.66	83.08	ND			ND	ND	ND	ND		
	12/14/06	10.49	82.24	ND			ND	ND	ND	ND		
	03/16/07	8.70	84.04	ND			ND	ND	ND	ND		
	06/21/07	6.59	86.15	ND			ND	ND	ND	ND		
	09/25/07	7.85	84.89	ND			ND	ND	ND	ND		
	12/21/07	5.76	86.98	ND			ND	ND	ND	ND		
	03/17/08	5.72	87.02	ND			ND	ND	ND	ND		
	06/16/08	6.20	86.54	ND			ND	ND	ND	ND		
	10/02/08	7.92	84.82	ND			ND	ND	ND	ND		
	12/04/08	7.09	85.65	ND			ND	ND	ND	ND		
	03/02/09	6.68	86.06	ND			ND	ND	ND	ND		
	06/11/09	6.29	86.45	<50			<1	<1	<1	<3		
	09/21/09	7.44	85.30	<50			<1.0	<1.0	<1.0	<3.0		
	12/07/09	7.68	85.06	<50			<1.0	<1.0	<1.0	<3.0		
	03/02/10	7.90	84.84	<50			<1.0	<1.0	<1.0	<3.0		
	09/26/11	9.21	83.53	<50			<1.0	<1.0	<1.0	<3.0	0.30	
	12/14/11	8.45	84.29	<50			<1.0	<1.0	<1.0	<3.0		

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-3	03/15/12	4.76	87.98	<50			<1.0	<1.0	<1.0	<3.0		
(Continued)	09/24/12	8.07	84.67	<50			<1.0	<1.0	<1.0	<3.0	<1.0	
	12/06/12	5.96	86.78	<50			<1.0	<1.0	<1.0	<3.0	<1.0	
	03/07/13	6.31	86.43	<50			<1.0	<1.0	<1.0	<3.0	<1.0	
	10/01/13	7.04	85.70	<50			<1.0	<1.0	<1.0	<3.0		
	07/06/15	7.39	85.35	<50			<1.0	<1.0	<1.0	<3.0		
	01/13/16	5.26	87.48									
	06/15/16	5.70	87.04	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	09/21/16	5.26	87.48									
	02/16/17	4.98	87.76	<50	<130	<250	3.5	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	7.46	85.28	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	NM										
	04/04/18	6.30	86.44	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	6.54	86.20	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	5.96	86.78	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/28/19	7.71	85.03	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-4	04/19/96			34,000			7,000	1,800	1,800	5,100		
92.27	05/16/97	4.12	88.15	11,300			3,800	26	432	1,490		
	04/06/00	4.17	88.10	7,500			2,000	25	130	110		
	07/20/00	4.48	87.79	1,600			2,500	82	670	1,900		
	11/17/00	4.63	87.64	8,700			2,200	20	210	130		
	02/27/00	4.52	87.75	13,000			850	ND	290	1,200		
	06/04/01	3.37	88.90	2,800			490	60	490	3,100		
	09/27/01	5.82	86.45	33,000			250	20	550	1,800		
	12/28/01	3.75	88.52	22,000			490	56	300	790		
	03/13/02	4.55	87.72	24,000			460	57	440	1,400		
	06/14/02	7.88	87.39	23,000			270	13	310	800		
	09/26/02	5.37	86.90	20,000			150	9	100	300		
	12/05/02	4.91	87.36	16,000			590	27	220	440		
	03/06/03	3.92	88.35	7,700			650	15	130	180		
	06/04/03	4.71	87.56	10,000			840	26	290	270		
	06/18/03	NM		76,900			2,310	8,290	3,900	19,800		
	07/01/03	NM		70,000			1,000	2,900	1,700	9,000		
	07/02/03	NM		97,000			1,700	4,800	2,900	14,000		
	09/10/03	7.47	84.88	NS			NS	NS	NS	NS		
	11/25/03	4.05	88.23	NS			NS	NS	NS	NS		
	02/26/04	4.40	87.87	NS			NS	NS	NS	NS		
	03/11/04	3.74	88.54	NS			NS 2.400	NS	NS	NS		
	06/16/05	4.00	88.27	52,000			3,400	300	6,200	6,200		

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-4	09/15/05	5.41	86.86	27,000			3,900	120	1,300	1,300		
(Continued)	12/15/05	4.26	88.01	38,000			4,200	100	1,500	2,200		
	03/16/06	6.62	85.65	5,800			450	36	160	610		
	06/12/06	5.21	87.06	18,000			3,600	130	1,400	900		
	09/26/06	5.61	86.66	22,000			2,600	54	770	610		
	12/14/06	2.99	89.28	41,000			1,100	190	910	2,800		
	03/16/07	6.79	85.48	37,000			2,500	550	1,200	2,900		
	06/21/07	5.10	87.17	41,000			2,300	400	1,500	3,000		
	09/25/07	7.03	85.24	8,600			870	42	410	270		
	12/21/07	4.05	88.22	160			ND	ND	ND	ND		
	03/17/08	4.08	88.19	4,700			53	8	47	35		
	06/16/08	7.30	84.97	7,700			670	30	400	190		
	10/02/08	7.13	85.14				Not sample	d due to sedir				
	12/04/08	7.41	84.86	6,000			950	25	220	68		
	03/02/09	5.97	86.30	5,200			1,200	16	110	41		
	06/11/09	6.40	85.87	4,500			1,300	200	170	66		
	09/21/09	6.49	85.78	3,100			890	10	91	<15		
	12/07/09	6.06	86.21	2,900			920	7.4	98	17		
	03/02/09	4.64	87.63	610			38	<1.0	10	<3.0		
	09/26/11	1.83	90.44	<50			<1.0	<1.0	<1.0	<3.0	< 0.30	
	12/14/11	5.13	87.14	250			130	<1.0	<1.0	<3.0		
	03/15/12	5.12	87.15	370			29	1.5	1	<3.0		
	09/25/12	6.72	85.55	1,100			340	25	7	15	<1.0	
	12/06/12	4.44	87.83	780			190	13	14	49	2.4	
	03/08/13	4.21	88.06	510			120	12	13	25	1.7	
	10/02/13	5.46	86.81	2,300			630	65	17	67		
	07/06/15	5.36	86.91	1,300			530	180	17	78		
	01/13/16	4.56	87.71									
	06/15/16	4.89	97.38	1,300	390	<250	580	56	19	130	<1.0	<1.0
	09/21/16	4.56	87.71									
	02/16/17	4.01	88.26	530	250	270	230	23	11	46	<1.0	<1.0
	10/24/17	5.35	86.92	1,500	560	280	710	71	26	120	1.2	<1.0
	01/17/18	4.06	88.21									
	04/05/18	4.16	88.11	1,800	460	290	1,000	270	29	130		
	07/24/18	5.96	86.31									
	02/18/19	3.01	89.26	370	540	530	440	37	8.4	35	<1.0	<1.0
	08/27/19	6.19	86.08	NS	NS	NS	NS	NS	NS	NS	NS	NS
MW-5	09/24/12	11.05	83.21	<50			<1.0	<1.0	<1.0	<3.0	<1.0	
94.26	12/06/12	9.08	85.18	140			42	<1.0	<1.0	12	<1.0	
	03/07/13	8.93	85.33	55			21	<1.0	<1.0	<3.0	<1.0	

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-5	10/01/13	9.76	84.50	53			9	<1.0	<1.0	<3.0		
(Continued)	07/06/15	10.38	83.88	<50			2	<1.0	<1.0	<3.0		
	01/13/16	9.02	85.24									
	06/15/16	9.95	84.31	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	09/21/16	9.02	85.24									
	02/15/17	8.65	85.61	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	10.29	83.97	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	8.85	85.41	<50	150	<250	<1.0	<1.0	<1.0	<3.0		
	04/03/18	9.05	85.21	<50	<150	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	10.59	83.67	<50	<150	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	8.83	85.43	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/28/19	10.71	83.55	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-6	09/24/12	11.09	82.46	<50			<1.0	<1.0	<1.0	<3.0	<1.0	
93.55	12/06/12	9.38	84.17	<50			<1.0	<1.0	<1.0	<3.0	<1.0	
	03/07/13	9.51	84.04	<50			<1.0	<1.0	<1.0	<3.0	1.3	
	10/01/13	10.13	83.42	<50			<1.0	<1.0	<1.0	<3.0		
	07/06/15	10.49	83.06	<50			<1.0	<1.0	<1.0	<3.0		
	01/13/16	9.45	84.10									
	06/15/16	10.09	83.46	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	09/21/16	9.45	84.10									
	02/14/17	9.11	84.44	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	10.69	82.86	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	9.30	84.25	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/04/18	9.52	84.03	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	10.79	82.76	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	9.28	84.27	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/28/19	10.95	82.60	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-7	09/25/12	8.24	83.30	410			2,100	4.9	4.3	13	<1.0	
91.54	12/06/12	6.09	85.45	800			1,700	6	12	18	<1.0	
	03/08/13	6.21	85.33	1,200			1,700	7.3	17	21	<1.0	
	10/02/13	6.88	84.66	1,200			1,500	6.7	13	16		
	07/06/15	7.53	84.01	1,200			1,400	15	12	24		
	01/13/16	6.09	85.45									
	06/15/16	6.95	84.59	2,000	660	<250	1,400	30	24	39	<1.0	<1.0
	09/21/16	6.09	85.45									
	02/16/17	5.94	85.60	2,600	680	<250	1,600	19	20	42	<1.0	<1.0
	10/24/17	7.43	84.11	3,900	640	<250	1,000	23	20	56	<1.0	<1.0
	01/17/18	5.98	85.56									
	04/06/18	6.20	85.34	2,700	1,100	<250	1,200	48	26	<3.0		
	07/24/18	7.71	83.83									

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-7	02/18/19	5.92	85.62	2,300	1,100	270	1,500	37	25	47	<1.0	<1.0
(Continued)	08/27/19	7.80	83.74	NS	NS	NS	NS	NS	NS	NS	NS	NS
MW-10	09/25/12	8.87	83.26	1,000			300	68	39	120	<1.0	
92.13	12/06/12	6.75	85.38	370			320	7.9	42	16	<1.0	
	03/08/13	6.90	85.23	830			530	9.0	110	30	<1.0	
	10/01/13	7.58	84.55	840			540	5.0	80	35		
	07/06/15	8.19	83.94	2,200			950	80	160	290		
	01/13/16	6.93	85.20									
	06/16/16	7.16	84.97	2,100	<130	<250	820	24	120	190	<1.0	<1.0
	09/21/16	6.93	85.20									
	02/16/17	6.39	85.74	2,100	210	<250	930	14	110	87	<1.0	<1.0
	10/24/17	8.26	83.87	1,800	210	<250	920	9.7	92	27	<1.0	<1.0
	01/17/18	6.90	85.23									
	04/06/18	6.84	85.29	1,600	410	<250	880	9.2	89	38		
	07/24/18	8.38	83.75									
	02/18/19	6.43	85.70	1,300	450	<250	880	4.4	56	21	<1.0	<1.0
	08/27/19	8.49	83.64	NS	NS	NS	NS	NS	NS	NS	NS	NS
MW-11	09/25/12	8.70	82.93	270			530	11	6.3	27	<1.0	
91.63	12/06/12	6.18	85.45	190			1,500	1.8	26	5.6	<1.0	
	03/08/13	6.90	84.73	930			1,900	5.8	110	110	<1.0	
	10/01/13	7.53	84.10	410			1,600	2.8	42	21		
	07/06/15	8.14	83.49	460			1,600	3.4	38	60		
	01/13/16	6.90	84.73									
	06/16/16	7.68	83.95	620	<130	<250	1,600	3.0	18	59	<1.0	<1.0
	09/21/16	6.90	84.73									
	02/16/17	6.45	85.18	300	<130	<250	1,300	1.0	1.9	5.2	<1.0	<1.0
	10/24/17	8.19	83.44	190	<130	<250	980	<5.0	<5.0	<15	<1.0	<1.0
	01/17/18	6.92	84.71									
	04/05/18	6.73	84.90	380	330	<250	1,100	1.7	3.3	11		
	07/24/18	8.24	83.39									
	02/18/19	6.63	85.00	350	480	<250	980	7.8	4.1	11	<1.0	<1.0
	08/27/19	8.30	83.33	NS	NS	NS	NS	NS	NS	NS	NS	NS
MW-12S	09/03/13	6.49	85.17	1,300			650	3	18	110		
91.66	10/01/13	6.06	85.60	4,600			630	<10	170	410		
	07/06/15	5.60	86.06	7,600			540	41	580	310		
	01/13/16	4.56	87.10									
	06/16/16	4.93	86.73	10,000	1,400	270	750	100	540	270	1.2	1.9
	09/21/16	4.56	87.10									
	02/16/17	4.33	87.33		-		Not sampled	due to heavy	hydrocarbon sheen	I		
	10/24/17	6.31	85.35	12,000	1,100	<250	960	61	470	200	<1.0	<1.0

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-12S	01/17/18	4.33	87.33									
(Continued)	04/03/18	4.21	87.45									
	07/24/18	5.82	85.84									
	02/18/19	3.62	88.04						hydrocarbon sheen	1		
	08/27/19	6.10	85.56	NS	NS	NS	NS	NS	NS	NS	NS	NS
MW-12D	09/03/13	7.96	83.67	90			1,500	2.3	1.2	<3.0		
91.63	10/01/13	7.10	84.53	65			1,400	2.0	<1.0	<3.0		
	07/06/15	7.72	83.91	120			1,200	2.5	<1.0	3.3		
	01/13/16	6.44	85.19									
	06/16/16	7.19	84.44	110	140	<250	980	2.0	1.3	<3.0	<1.0	<1.0
	09/21/16	6.44	85.19									
	02/16/17	6.00	85.63	220	180	<250	1,200	1.5	<1.0	4.4	<1.0	<1.0
	10/24/17	7.62	84.01	72	160	<250	550	<5.0	<5.0	<15	<1.0	<1.0
	01/17/18	6.18	85.45									
	04/06/18	6.40	85.23	290	870	<250	980	1.8	<1.0	5.5		
	07/24/18	7.90	83.73									
	02/18/19	6.17	85.46	200	850	<250	1,000	2.0	<1.0	5.0	<1.0	<1.0
	08/27/19	6.85	84.78	NS	NS	NS	NS	NS	NS	NS	NS	NS
MW-13	01/13/16	5.56	84.75	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
90.31	06/14/16	6.01	84.30	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
50.01	09/21/16	5.56	84.75									
	02/15/17	5.12	85.19	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	6.40	83.91	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	5.40	84.91	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/04/18	5.67	84.64	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	6.48	83.83	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	5.25	85.06	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/29/19	6.68	83.63	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-14	01/13/16	7.55	83.87	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
91.42	06/14/16	6.15	85.27	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
31.42	09/21/16	7.55	83.87									
	02/15/17	7.03	84.39	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	8.10	83.32	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	04/05/18	7.53	83.89	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	8.79	82.63	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	6.91	84.51	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/29/19	8.71	82.71	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
<u>MW-15</u>	01/17/18	7.08	84.34	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
90.62	01/13/16	4.96	85.66	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	06/14/16	6.19	84.43	<50	160	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-15	09/21/16	4.96	85.66									
(Continued)	02/15/17	4.91	85.71	<50	150	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	6.28	84.34	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	4.72	85.90	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/05/18	5.04	85.58	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	7.02	83.60	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	4.58	86.04	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/29/19	5.79	84.83	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-16	00/04/40	0.74	00.05	50	100	050	1.0	1.0	1.0		1.0	1.0
-	09/21/16	9.74	82.65	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
92.39	02/15/17	7.43	84.96	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	9.73	82.66	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	7.76	84.63	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/04/18	7.82	84.57	<50	220	300	<1.0	<1.0	<1.0	<3.0		
	07/24/18	8.83	83.56	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	8.30	84.09	<50	240	330	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/29/19	8.94	83.45	<50	150	<250	<1.0	<1.0	<1.0	<3.0		
MW-17	09/21/16	8.89	84.95	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
93.84	02/14/17	7.61	86.23	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	7.88	85.96	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	7.62	86.22	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/04/18	8.22	85.62	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	8.85	84.99	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	12/18/19	7.42	86.42	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/29/19	8.68	85.16	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-18	09/21/16	8.62	82.75	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
91.37	02/15/17	5.13	86.24	<50	140	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	10/24/17	6.97	84.40	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	5.19	86.18	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/05/18	5.48	85.89	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	7.32	84.05	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	02/18/19	5.19	86.18	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/30/19	7.07	84.30	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-19	09/21/16	5.50	86.71	120	<130	<250	200	<1.0	<1.0	3.8	<1.0	<1.0
92.21	02/16/17	7.05	85.16	90	180	<250	110	<1.0	<1.0	<3.0	<1.0	<1.0
32.21	10/24/17	9.03	83.18	74	140	<250	88	<1.0	<1.0	3.3	<1.0	<1.0
	01/17/18	6.39	85.82			~230						
	04/05/18	5.94	86.27	70	600	280	63	<1.0	<1.0	<3.0		
	07/24/18	7.88	84.33									
	02/18/19	6.30	85.91	73	730	<250	52	<1.0	<1.0	<3.0	<1.0	<1.0
	08/27/19	8.14	84.07	NS	NS	NS	NS	NS	NS	NS	NS	NS

Well ID	Sample Date	Depth to Water	Groundwater Elevation	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes	Total Lead	Dissolved Lead
MW-20	02/15/17	5.70	86.17	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
91.87	10/24/17	7.23	84.64	<50	<130	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	01/17/18	5.81	86.06	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	04/05/18	6.06	85.81	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
	07/24/18	7.74	84.13	<50	<130	390	<1.0	<1.0	<1.0	<3.0		
	02/18/19	5.56	86.31	<50	140	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
	08/30/19	7.82	84.05	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-21	02/18/19	5.16	86.67	58,000	3,900	320	4,300	6,700	1,400	6,800	1.1	<1.0
91.83	08/28/19	7.19	84.64	200,000	3,100	450	14,000	23,000	4,300	24,000		
MW-22	02/18/19	11.12	81.44	<50	350 *	280 *	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
92.56	08/29/19	9.22	83.34	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-23	02/18/19	4.86	87.16	<50	190 *	<250 *	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
92.02	08/30/19	8.14	83.88	<50	<130	<250	<1.0	<1.0	<1.0	<3.0		
MW-24	02/18/19	9.75	83.48	<50	180	<250	<1.0	<1.0	<1.0	<3.0	<1.0	<1.0
93.23	08/28/19	9.24	83.99	<50	140	<250	<1.0	<1.0	<1.0	<3.0		
SVE-1	10/01/13	5.63	85.68	100,000			7.100	9,300	2,600	13,000		
91.31	07/06/15	4.69	86.62	100,000			mpled due to			13,000		
51.01	01/13/16	3.52	87.79									
	06/16/16	4.03	87.28	100,000	1,600	290	9,600	3,000	3,400	15,000	2.1	3.4
	09/21/16	3.52	87.79									
	02/17/17	2.98	88.33			I	Not sampled	due to heavy	hydrocarbon sheer			I
	10/24/17	6.14	85.17	65,000	1,500	320	7,800	160	2,800	6,900	1.1	<1.0
	01/17/18	3.39	87.92						,000			
	04/03/18	3.49	87.82									
	07/24/18	4.97	86.34									
	02/18/19	2.91	88.40		•	•	Not sampled	due to heavy	hydrocarbon sheer	1	•	•
	08/27/19	5.30	86.01	NS	NS	NS	NS	NS	NS	NS	NS	NS
SVE-2	10/01/13	6.01	85.53	140,000			11,000	13,000	3,100	19,000		
91.54	07/06/15	5.54	86.00			Not sa	mpled due to	heavy hydrod	arbon sheen			•
	01/13/16	4.35	87.19									
	06/16/16	4.75	86.79	120,000	1,900	<250	11,000	5,900	3,200	16,000	<1.0	<1.0
	09/21/16	4.35	87.19									
	02/17/17	3.99	87.55			Not sampled	due to heavy	hydrocarbon	sheen			
	10/24/17	7.08	84.46	80,000	2,500	1,000	8,700	1,600	2,200	9,400	<1.0	<1.0
	01/17/18	4.35	87.19									
	04/03/18	9.32	82.22									
	07/28/18	5.69	85.85									
	02/18/19	3.81	87.73				Not sampled		hydrocarbon sheer	<u> </u>		
	08/27/19	5.98	85.56	NS	NS	NS	NS	NS	NS	NS	NS	NS

UST WELL	06/25/13	4.10	87.52	16,000			40	7.2	23	1,100		
91.62	10/01/13	4.93	86.69	30,000			76	13.0	56	2,000		
	07/06/15	4.81	86.81	7,300			88	11.0	32	38		
VAULT-1	10/02/13	5.63	85.79	210			130	1.5	5.4	<3.0		
91.42	07/06/15	4.79	86.63	520			630	23	9.9	53		
VAULT-2	10/02/13	4.74	85.35	3,900			580	51	110	220		
90.09	07/06/15	4.33	85.76	440			78	12	18	30		
VAULT-3	10/02/13	2.90	88.37	<50			<1.0	<1.0	<1.0	<3.0		
91.27	07/06/15	5.31	85.96	<50			<1.0	<1.0	<1.0	<3.0		
MTCA Metho	od A Cleanup	Levels:		1,000/800 <sup>1</sup>	500	500	5	1,000	700	1,000	15	15

TPH-G Total petroleum hydrocarbons as gasoline analysis using Ecology Method NWTPH-G

TPH-D Total petroleum hydrocarbons as diesel analysis using Ecology Method NWTPH-Dx

TPH-O Total petroleum hydrocarbons as oil analysis using Ecology Method NWTPH-Dx Benzene, toluene, ethylbenzene and total xylenes analysis using EPA Method 8021 Total and dissolved lead analysis using EPA Method 200.8

ND<50 Not detected at or above the indicated method reporting limit

ND Not detected. Method reporting limit not indicated in prior consultants' reports.

NM Not measured

-- Not applicable or no data

1 Benzene detected/benzene not detected and the sum of toluene, ethylbenzene and total xylenes concentrations is less than 1% of the gasoline mixture Top of casing elevation indicated below Well ID Depths are in feet below top of casing

Groundwater elevations are relative to an established datum at an assigned elevation of 100 feet above mean sea level.

Results in micrograms per liter (ug/L)

Bolded and shaded values exceed MTCA Method A cleanup levels

Data prior to 1/13/16 are taken from prior consultants' reports

NS Not sampled

\* Resampled on 2/23/19 due to laboratory breakage

## Table 2 **Groundwater Sample Analytical Results Drilling and Well Installation** Mercer Island Shell (Former BP) 7833 SE 28th Street Mercer Island, Washington

Sample Name	Sample Date	EDB	EDC	МТВЕ	PAHs	VOCs	PCBs	Pesticides
MW-1	01/30/19	NS	NS	NS	NS	NS	NS	NS
	08/24/19	<2.0	<2.0	ND	NS	NS	NS	NS
MW-5	01/30/19	NS	NS	NS	NS	NS	NS	NS
	08/24/19	<2.0	<2.0	ND	NS	NS	NS	NS
MW-6	01/30/19	NS	NS	NS	NS	NS	NS	NS
	08/24/19	<2.0	<2.0	ND	NS	NS	NS	NS
MW-24	01/30/19	<2.0	<2.0	2.6	ND	ND	ND	ND
	08/24/19	<2.0	<2.0	2.2	NS	NS	NS	NS
Model Toxics Cor (MTCA) Method A Level		0.01	5	20	Various	Various	Various	Various

Dibromomethane (EPA-8260) EDB

EDC Dichloroethane (EPA-8260)

MTBE Methyl Tertiary-butyl Ether (EPA-8260)

Polycyclic aromatic hydrocarbons (EPA-8270 SIM) Volatile organic compounds (EPA-8260) Polychlorinated biphenyls (EPA-8082) PAHs

VOCs

PCBs

DEHP Bis (2-ethylhexyl) phthalate (EPA-8270)

<2.0 Not detected at or above the indicated method reporting limit

ND Not detected

Not sampled NS

Results are in micrograms per liter (ug/kg) Depths are in feet below ground surface

Bolded and shaded values exceed MTCA Method A cleanup levels

Table 3         Cost Estimate         Site Remediation         Mercer Island Shell         7833 SE 28th Street         Mercer Island, Washington													
	Unit Type	Units		Unit Cost		Total							
Scope of Work: Excavate and remove up to 1,500 cubic yards (2,000 t removal of the existing tanks and piping; remove and replace existing quarterly monitoring and sampling to document groundwater cleanu Insurance Agency for issuance of a No Further Action determination.	g groundwater moi p; compile data an	nitoring wells in the exc	avated	l area; condu	uct 2	2 years of							
Site Preparation													
Permitting, Fencing, Traffic Control, Concrete and Asphalt Removal	Estimate	1	\$	45,000.00	\$	45,000.00							
Tank Decommissioning and Removal, Dispenser and Piping Removal*	Estimate	1	\$	60,000.00	\$	60,000.00							
* Not including installation of new tanks and lines		Site Pr	eparat	ion Subtotal	\$	105,000.00							
Soil Excavation and Cleanup													
Project Manager	Hrs	80	\$	110.00	\$	8,800.00							
Field Supervisor	Hrs	80	\$	95.00	\$	7,600.00							
Senior Technician	Hrs	80	\$	80.00	\$	6,400.00							
Excavator	Day	10	\$	900.00	\$	9,000.00							
Dumptucks (3 trucks with trailer each day)	Day	10	\$	2,400.00	\$	24,000.00							
Shoring Materials and Foundation Supports (if needed)	Estimate	1	\$	80,000.00	\$	80,000.00							
Disposal Fees	Ton	2,000	\$	55.00	\$	110,000.00							
Backfill Material and Placement	Ton	1,600	\$	45.00	\$	72,000.00							
Excavation Water	Gallon	10,000	\$	1.00	\$	10,000.00							
Remove and Replace Monitoring Wells	Estimate	1	\$	60,000.00	\$	60,000.00							
Quarterly Groundwater Monitoring	Estimate	1	\$	80,000.00	\$	80,000.00							
Final Cleanup Oversight and Reporting, Well Decommissioning	Estimate	1	\$	60,000.00	\$	60,000.00							
		Soil Excavation and	d Clear	nup Subtotal	\$	527,800.00							
				Subtotal	\$	632,800.00							
		(	Conting	gency (10%)	\$	63,280.00							
		Sub	total B	efore Taxes	\$	696,080.00							
			Sales	Tax (10.1%)	\$	70,304.08							
		То	tal Est	imated Cost	\$	766,384.08							

**PROJECT**:

# BP Branded Service Station

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W.O. 11-10706-00 WELL NO.MW-1

Elevatio Ground		Vell completed: axing elevation:				95	AS-BUILT DESIGN	Page 1 of 1
(PEPTH (feet)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	BLOW	OVM READING	GROUND	Flush-mounted steel monument	TESTINO
- 0 -	2.5' Asphalt Paving over soft, wet, sandy SLT with some gravel and b fragments (FB) Very stiff, moist, tan-gray motified, sandy SLT (no odor)	brown. rick	S-) '	30	0		Ground surface Top of casing Cement Bentonite	
- 5 -	Becomes hard, with trace fine gra odor)	wel (no	S-2	38	-		Cosing (Schechule-40 2-inch I.D. PVC)	WITH-O WITH-O BS Tong Loog
- 10 -	Very stiff, most, gray, fine sandy S grading to medium dense, wet, g slity, fine to medium SAND (no od Very dense, saturated, gray, fine s	ray.	5-3	18	0		10-20 sand Alter pack Screen (2-Inch I.D. PVC with 0.01-inch slots)	-
- 20 -	(no odor)		S-4	45	0		Threaded end cap	
- 25 ·	Bottom of boring at 20 feet.							
AGRA Earth and Environmental		Cosserver acato 0/00/00 = withing withing bat fabriliand	l grouni date o alytical	Caervor	leve) d	- <b></b>	AGRA Earth & Environmental 11335 NE 122ad Way, Suite 100 Kirkland, Washington 98034-6918	<b>.</b>

Drilling stated - 27 December 1006

Delline semalaride of December 1000

**PROJECT:** 

## BP Branded Service Station

## W.O. 11-10706-00 WELL NO.MW-2

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Elevation Ground	a reference: 100.00 tool temporary benchmark surface elevation:96.65 feet	Well complete Casing clever				**5	AS-BUILT DESIGN	Page 1 of 1
DEPTH (ted)	SOIL DESCRIPTION	SAMPLE	TYPE SAMPLE	BLOW	0VM READING	GROUND	Flush-mounted steel manument	TESTING
- 5 -	13° Asphalt Paving Solt, wet, blue-gray, sandy, clay with fine gravel and wood fragi (slight gasoline-like odor) Soft to mealum stiff, wet, green- clayey SILT with some fine sand rootlets (slight gasoline-like odor	-oray, and	3.0 5-1		65 42	12/20,000	Giound surface Top of casing Cerment Bentonite Casing (Schedule-40 2-Inch I.D. PVC)	WTH-O WTH-O DE Real Lood
- 10 -	Very silff, moist, gray SLT with th and fine gravel (no odor)	ace sand	5-2	30	0		10-20 sand filter pack	
- 15 -	Becomes hard, molst, sandy SIL odor)	J (no	s.	JZ	0		Screen (2-Inch I.D. PVC with 0.01-Inch slots)	
- 20 -	Becomes very hard, molst, fine SILT with sand (no odor)	, gravelly	s∽	4 50	0	+		
- 25 -	Bottom of boring at 20.9 fe	et.						
- 30 -	LEGEND 2 Jinch O.D. 1 Spiritepoon sample Grab sample Collegend groundwater level ATD = of time of dring Diffice started: 27 Decomptor 1005	ACOVED D/00 WITH-D Ext. Total Lead	erved grok /00 = dicte Analytic	obeerve	d		AGRA Earth & Environmental 11335 NE 122nd Way, Suite 100 Kirkland, Washington 98034-6918	Į

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07/25/2007 11:47 AM

**PROJECT:** 

## BP Branded Service Station

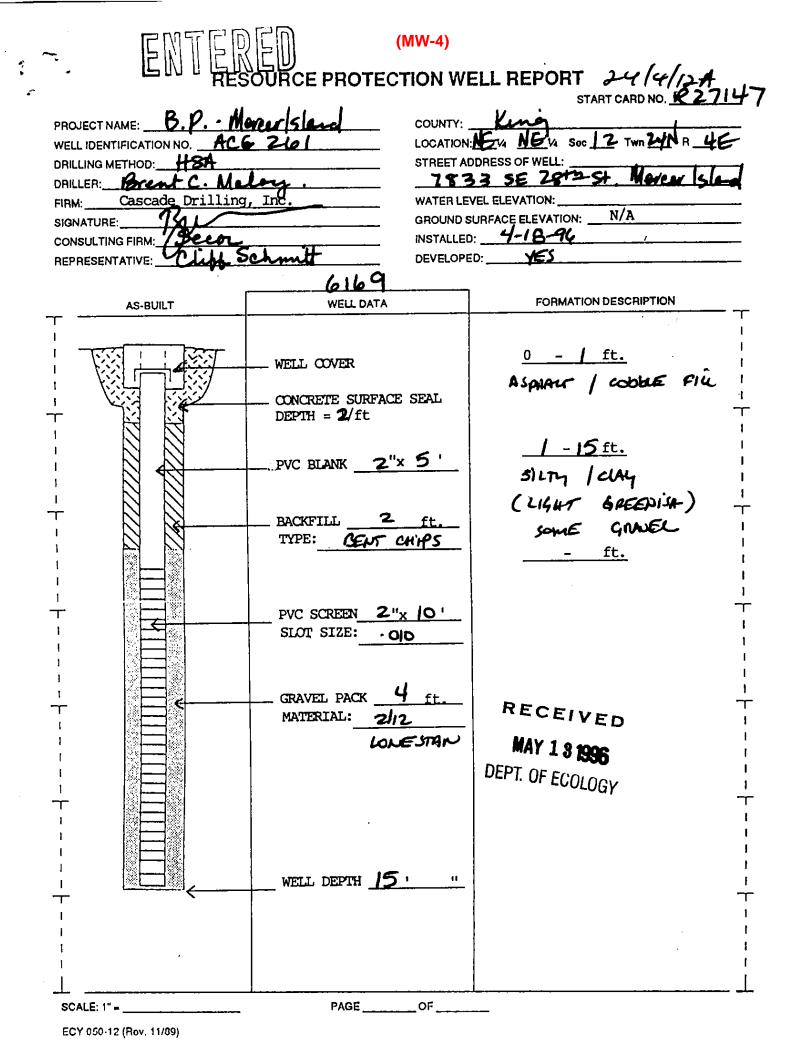
W.O. 11-10706-00 WELL NO.MW-3

Elevation reference: 100.00 loot temporary	Well completed			ber 19	95	AS-BUILT DESIGN	Page 1
Ground surface elevation:97.83 (66)	Casing elevation		feet			AS-BOILT DESIGN	of 1
SOIL DESCRIPTION	SAMPLE	SAMPLE NUMBER	BLOW	OVM READING	GROUND WATER	Fush-mounted steel monument	TESTINO
0 7' Asphalt Paving						Ground surface	
Hard, moist, tan mottled \$LT wil gravel and sand (no odor)	h trace	S-1	42	0	•	Cement Bentonite Casing (Schedule-40	WITH-O BAL Bota Lood
Becomes clark gray (no odor)	-			-		2-Inch I.D. PVC)	
- 10 -		S-2	37	0			
						10-20 sand filter pack	
- 15 -		S-3	39	0	∮ ↓ ≁	Screen (2-Inch I.D. PVC with 0.01-inch slots)	
Becomes very sliff (no odor)	]						
- 20		5-4	29	0		Threaded end cap	
Bottom of boring at 20 feet							
- 25 -			+		+		
					•		
30     LEGEND       1     24nch O.D.       1     1pillspoon sample       3     Grab sample       3     Observed groundwater level       3     AD		id ground = date of natytical !		loval 1		AGRA Earth & Environmental 11335 NE 122nd Way, Suite 100 Kirkland, Washington 98034-6918	<b>-</b>

Drilling stated: 28 December 1005

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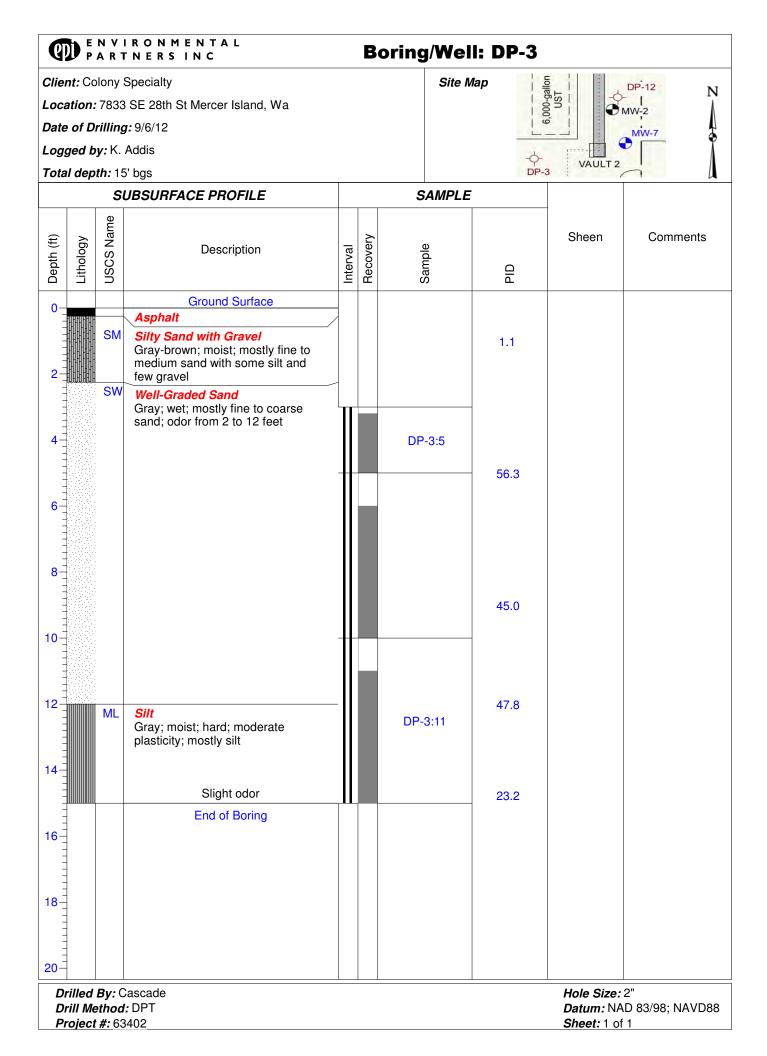
Delline equaleted. 00 Due ------



The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

Ø	D E P	N V A R T	IRONMENTAL INERSINC		B	Boring/Wel	l: DP-1		
Clier	nt:Co	lony	Specialty			Site M	lap _		N
Loca	ation:	7833	BSE 28th St Mercer Island, Wa				6,00	MW-4	
Date	of Di	rilling	<b>g:</b> 9/6/12						MALK
Logg	ged b	<b>y:</b> K.	Addis					ÅГ Г	SIDE WALK
Tota	l dep	th: 15	5' bgs				DP-1		
		S	UBSURFACE PROFILE			SAMPLE			
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Sample	OLA	Sheen	Comments
0-			Ground Surface						
			Crushed Rock	Н					
2		SM GP	<i>Silty Sand</i> Gray-brown; moist; mostly sand with some silt <i>Pea Gravel</i> Gray; dry; mostly fine gravel	-		DP-1:2.5	21.6		
6 6		SM	Sandy Silt Gray-brown; moist; mostly silt with some fine sand				14.7 7.6		
8		GP SM	<i>Fill</i> Black; rust-stained; mostly gravel with some charcoal and debris <i>Silty Sand</i> Tan; dry; silty sand with few gravel; becomes moist and gray	-			18.6		
10		SM	Becomes gray-brown <i>Silty Sand</i> Gray; moist; mostly silt with little sand and trace clay	-			20.2		
14		SM	<i>Silty Sand</i> Brown; moist; mostly fine to medium sand with some silt				50.0		
14		MH SP	Elastic Silt         Gray; damp; mostly silt         Poorly-Graded Sand	- 		DP-1:15	71.2		Saturated at 14.8
16			Gray; saturated; mostly fine to medium sand with trace silt End of Boring						
Dı Dı	rill Me	thod	Cascade I: DPT 3402.0	<u> </u>	<u> </u>			Hole Size: Datum: NA Sheet: 1 of	D 83/98; NAVD88

QĮ	D P		RONMENTAL NERSINC		В	oring/Well	: DP-2		
Clier	nt: Co	olony S	Specialty			Site Ma			Ν
oca	tion:	7833	SE 28th St Mercer Island, Wa				-\$-	Lo I	
ate	of D	rilling	: 9/6/12					6,000-gallon UST	
ogg	ged b	<b>y:</b> K. /	Addis					6,00	/W-4
ota	l dep	<b>th:</b> 15	1					0	€ L
		รเ	JBSURFACE PROFILE			SAMPLE			
		ne							
Ueptn (tt)	Lithology	USCS Name	Description	Interval	Recovery	Sample	DIA	Sheen	Comments
0-			Ground Surface						
2		SM GP	Asphalt Silty Sand Gray-brown; moist; mostly fine to medium sand with some silt and little gravel	/		DP-2:3	1.7		
4			<i>Pea Gravel</i> Odor			UF-2.0	31.6		DUP-1
			Strong odor			DP-2:9	34.5		
8		SP- SM	Strong odor Poorly-Graded Sand with Silt Gray-brown; saturated; mostly coarse sand with some silt; strong	/			40.2		
2 4		МН	odor Elastic Silt Gray; damp; hard; high plasticity; mostly silt/clay; no odor				0.9		
6 0			End of Boring				1.1		Refusal at 15
Dr Dr	'ill Me	<b>By:</b> C ethod			<u> </u>			Hole Size: Datum: NA Sheet: 1 of	D 83/98; NAVD8



Q	Denvironmental Boring/Well: DP-4												
Clier	nt: Co	olony	Specialty			Site	Мар		N				
Loca	ation:	7833	SE 28th St Mercer Island, Wa				DP-5	L					
			<b>1:</b> 9/6/12				]						
			Addis										
Tota	i aep	th: 10	UBSURFACE PROFILE			SAMPL	F		Ц				
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Sample	OId	Sheen	Comments				
0-			Ground Surface										
2		ML	Concrete Silt with Sand Mottled gray; moist; mostly silt with few sand and trace gravel										
4			Slight odor			DP-4:2.5	15.4						
6		ML	<i>Silt with Sand</i> Brown-gray; moist; mostly silt with few sand and few gravel				16.8						
8			No odor			DP-4:7.5	0.1		Potucol et 10'				
10-			End of Boring				0.4		Refusal at 10'				
12-													
14-													
-													
16													
18-													
20-													
Di	Drilled By: Cascade         Hole Size: 2"           Drill Method: DPT         Datum: NAD 83/98; NAVD88           Project #: 63402         Sheet: 1 of 1												

Ø	D F P	N V I A R T	RONMENTAL NERSINC	Boring/Well: DP-5					
Clier	nt: Co	olony	Specialty			Site N	lap		N
Loca	ation	7833	SE 28th St Mercer Island				<b>5-5</b> -∲-		
Date	of D	rilling	<b>1:</b> 9/6/12			DF	<b>⊳-5</b> '\'	r_n	<sup>-</sup> <b>DP-4</b>
		<b>у:</b> К							
Tota	l dep	th: 10							A
			JBSURFACE PROFILE			SAMPLE			
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Sample	CIA	Sheen	Comments
0-			Ground Surface				-		
2		ML	Asphalt Sandy Silt Brown-gray; moist; mostly silt with some fine sand	/					
4		MH	<i>Elastic Silt</i> Brown-gray; moist; mostly silt and/or clay	_		DP-5:4	0.0		
6 		ML	<i>Silt with Sand</i> Brown-gray; moist; mostly few silt with few sand						
		MH	<i>Elastic Silt</i> Brown-gray; moist; mostly silt and/or clay			DP-5:9	0.0		
12-14-16-18-18-18-18-18-18-18-18-18-18-18-18-18-			End of Boring						
Dr	rill Me	<b>By:</b> C ethod t #: 63						Hole Size: Datum: NA Sheet: 1 of	D83/98; NAVD88

ENVIRONMENTAL PARTNERS INC	Boring	/Well: DP-6	
Client: Colony Specialty		Site Map	N
Location: 7833 SE 28th St Mercer Island		DP-6	
Date of Drilling: 9/6/12			DP-7 ↔ B-2 ⊗
Logged by: K. Addis Total depth: 10'			
SUBSURFACE PROFILE	S	AMPLE	
Depth (ft) LLithology USCS Name USCS Name	Interval Recovery Samole	Да	Sheen Comments
0 Ground Surface			
0       Asphalt         Silty Sand         Silty Sand with gravel         Elastic Silt         Brown-gray; moist; mostly silt         and/or clay moderate to high         plasticity         4         6         8         10         Becomes gray         End of Boring         12         14         16	DP-6	0.0	
18       20       Drilled By: Cascade       Drill Method: DPT       Project #: 63402			Hole Size: 2" Datum: NAD83/98;NAVD88 Sheet: 1 of 1

lier	nt: Co	lony \$	Specialty			Site Ma	р	i	
			SE 28th St Mercer Island				DP-6		]
ate	of D	rilling	<b>g:</b> 9/6/12						P 2 -
			Addis					DP-7 Y	B-2⊗
			)' bgs					Ĵ	
			UBSURFACE PROFILE			SAMPLE			
		e							
הפשווו (וון)	Lithology	USCS Name	Description	Interval	Recovery	Sample	DIA	Sheen	Comments
)_			Ground Surface						
-		N AL	Asphalt	/					
		ML	Silt with Sand Brown-gray; moist; mottled; mostly silt with few fine sand	/					
11111		СН	<i>Fat Clay</i> Brown-gray; moist; hard; mostly clay; moderate plasticity; mottled						
			day, moderate plasticity, motied						
						DP-7:5	0.0		
 		СН	Fat Clay			DP-7:10	0.0		
-			Gray; moist; hard; mostly clay	1					
-			End of Boring						
2									
-									
-									
-									
-									
-									
5-									
-									
3-									
-									
- - - - (									
	illed	<b>By:</b> C	Cascade	<u> </u>				Hole Size: 2	2"
			: DPT					DetumeNA	D 83/98; NAVD8

lier	nt• Co	Nonv S	Specialty			Site I	<i>l</i> an	MW-1	
			SE 28th St Mercer Island			One h	μαρ	VAULT 1	<sup>7</sup> • I
			1:9/6/12						
		у: К. /					B-3 ⊗	DP-8_	
		<i>th:</i> 10							1
	•		JBSURFACE PROFILE			SAMPLE			
		e						_	
ni) IIIdan	Lithology	USCS Name	Description	Interval	Recovery	Sample	QL	Sheen	Comments
)_			Ground Surface						
			Concrete	/					
2		GW	<i>Sandy Gravel</i> Brown; moist; mostly fine to coarse gravel with some sand				3.7		
4		MH	<i>Elastic Silt</i> Gray; moist; mostly silt; odor; reworked silt; fill			DP-8:4	399		
6 1111111		MH	<i>Elastic Silt</i> Gray; saturated; mostly silt and clay; strong odor; fill						
3		MH	<i>Elastic Silt</i> Brown-gray; moist; mostly silt and clay; no odor	-		DP-8:7	1729		DUP-2
			End of Boring				0.2		
2									
- - - 4-									
5									
3- - -									
		By: C ethod	ascade					Hole Size:	2" D83/98; NAVD8

Q	D P	N V I A R T	RONMENTAL NERSINC	Boring/Well: DP-9							
Clier	nt: Co	olony	Specialty			Site N	Мар		N		
Loca	ation:	7833	SE 28th St Mercer Island				MAI 10 2		N		
Date	of D	rilling	<b>:</b> 9/6/12				MW-10		DP-9		
Log	ged b	<b>у:</b> К.	Addis						······		
Tota	l dep	th: 15									
		Sl	JBSURFACE PROFILE			SAMPLE		-			
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Sample	DIA	Sheen	Comments		
0-			Ground Surface				-				
2		CL	Asphalt Lean Clay Gray-green; moist; mostly lean clay				2260				
		ОН	<i>Silt</i> Black; moist; mostly organic silt; charcoal; odor			DP-9:3	6800				
4		ML	Silt Elastic silt; moist; brown-green with few sand, gravel and roots; odor				- 5200				
6 		SM	Becomes gray-green; odor <i>Silty Sand</i> Gray; moist; very dense; mostly fine sand with some silt and few gravel			DP-9:7.5	2180				
10		MH	<i>Elastic Silt</i> Gray-green; moist; mostly elastic silt; slight odor								
12		MH	<i>Elastic Silt</i> Gray; hard; mostly silt				_				
			End of Boring			DP-9:15	1900				
16			End of Borning								
18-											
-											
20-											
Dı	Drilled By: Cascade         Hole Size: 2"           Drill Method: DPT         Datum: NAD83/98; NAVD88           Project #: 63402         Sheet: 1 of 1										

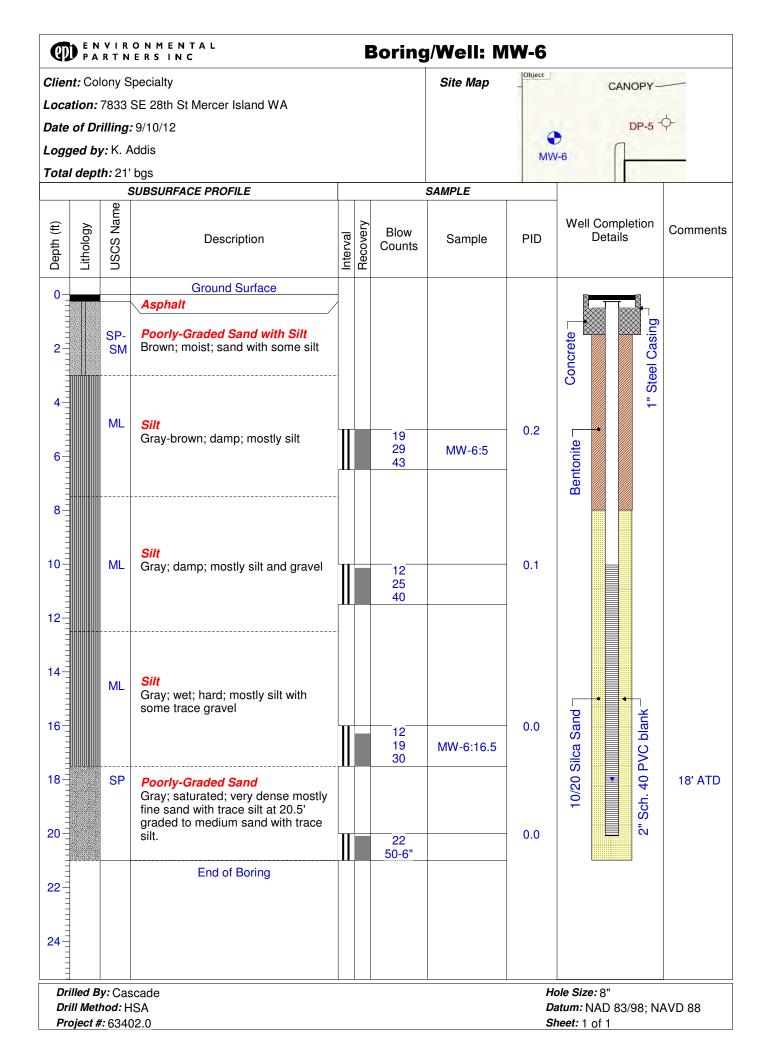
Q	PARTNERS INC Boring/Well: DP-10											
Clier	nt: Co	olony	Specialty				Site M	lap	DP-11	N		
Loca	ation	7833	SE 28th St Mercer Island, Wa							N		
Date	e of D	rilling	<b>1:</b> 9/6/12					DP-1	°	Ą		
			Addis					s-1 ⊗ Rettor	I Fenter	Ā		
Tota	l dep	th: 10						·		Д		
			UBSURFACE PROFILE			S.	AMPLE					
t)	~	USCS Name			2	<b>`</b>			Sheen	Comments		
Depth (ft)	Lithology	CS N	Description	Interval	Recoverv		2					
Dep	Lith	NSI		Inte	Bec		5	PID				
0-			Ground Surface									
=		SM	Concrete Silty Sand	-						Hand cleared to 4'		
			Gray-mottled; moist; mostly silt with some sand and few gravel									
2-			Some sand and for graver			DP-1	0.0 F	56.9				
						DP-1	0.2.5	56.9				
4												
-								2171				
6												
				+		DP-	10.8					
8-	-	ML	Silt with Sand				10.0	3400				
-	-		Tan; moist; mostly silt with some sand and trace gravel									
10-								2500				
			End of Boring									
12	-											
14-												
=	-											
16-												
18-												
20-												
	rilled	By: C	ascade						Hole Size:	2"		
D	rill Me	ethod	: DPT						Datum: NA	D83/98; NAVD88		
PI	ojeci	#: 63	94UZ						Sheet: 1 of			

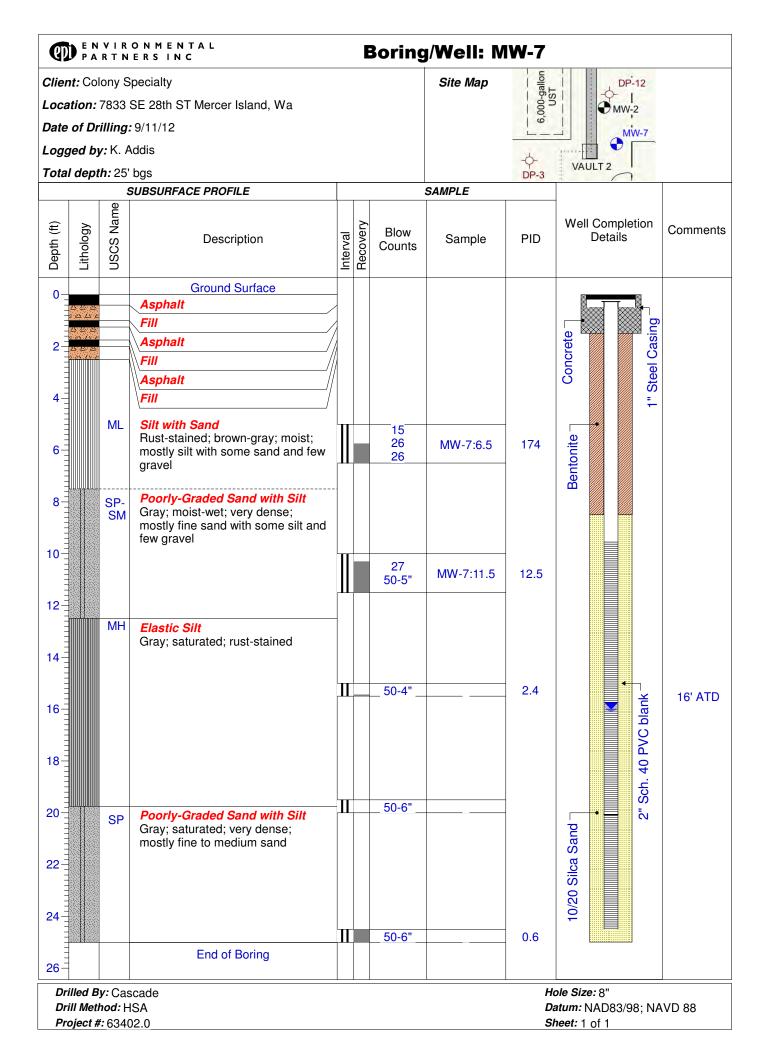
Q	PARTNERS INC Boring/Well: DP-11											
Clier	nt: Co	olony	Specialty				Site M		DP-11			
			SE 28th St Mercer Island, Wa						_	N		
			<b>9</b> /6/12					DP-	10	A		
		у: К.						1-1 ⊗		9		
		<i>th:</i> 10							m <del>Center</del>			
			UBSURFACE PROFILE			S	AMPLE	· <b>庙</b>		и		
lf)	2	USCS Name			2				Sheen	Comments		
Depth (ft)	Lithology	SC	Description	Interval	Recovery							
Dep	Lith	NS(		Inte	Rec	U S	3	DID				
0-			Ground Surface									
	HÚHHÚHHÚF		Landscaping Bark	-								
2		SM	<i>Silty Sand</i> Tan; damp; mostly silty sand with trace gravel			DP-	11:3					
		ML	Silt with Sand	-11				26				
4-			Gray; moist; mostly silt with 2" sand seam at 4.5'					3				
6		ML	<i>Silt with Sand</i> Brown; damp; mostly silt with 1" sand seam at 8'			DP-	11:5	3				
8			Increasing gravel					4				
10			End of Boring					3				
	-											
12-												
14-												
16-												
18-												
20												
Di Di	rill Me	ethod	cascade : DPT							D83/98; NAVD88		
Pr	roject	#: 63	402						Sheet: 1 of	1		

Ø	D E P	N V I A R T								
Clier	nt: Co	lony S	Specialty				Site M		DP	-12 N
Loca	ation:	7833	SE 28th St Mercer Island					ap (6,000-gallon	MW-	
Date	of D	rilling	<b>y:</b> 9/6/12					9		W-7
	-	-	Addis					-\$-	VAULT 2	
Tota	l dep	th: 15						DP-3		
			UBSURFACE PROFILE	SAMPLE						
Depth (ft)	Lithology	USCS Name	Description	Interval	Recoverv			Old	Sheen	Comments
0-			Ground Surface							
2		SM	Asphalt Silty Sand Brown-mottled orange; damp; mostly fine to medium silty sand with gravel			DP-	12:3	0.0		
6		MH	<i>Elastic Silt</i> Gray; moist; saturated; high plasticity; mostly silt	,		DP-	12:6			
		SP	<b>Poorly-Graded Sand</b> Gray; saturated; medium dense; mostly fine to medium sand					12.0		
		SP	<b>Poorly-Graded Sand with Gravel</b> Mottled gray; moist; very dense; mostly fine to medium sand with gravel	-				4.0		
10		MH	<i>Elastic Silt</i> Gray; moist; high plasticity; mostly silt							
12								0.0		
			End of Boring							
16										
Dr	rill Me		cascade : DPT :402						Hole Size: Datum: NA Sheet: 1 of	D 83/98; NAVD88

Q	D P	N V A R T	IRONMENTAL TNERSINC	oring/Wel	I: HSA	-1			
Clie	nt: Co	lony	Specialty			Site N	Лар		N
Loca	ation:	7833	SE 28th ST, Mercer Island, Wa					🛞 HSA-1	I A
			<b>g:</b> 9/10/12						\$
			Addis						<u>-</u> \
Tota	l dep		)' bgs				-		Ц
			UBSURFACE PROFILE			SAMPLE	:		
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Sample	OId	Sheen	Comments
0	20029 20030 20000 20000 20000 200000000	GP	Ground Surface <b>Poorly-Graded Gravel with Sand</b> Brown; moist; mostly fine gravel with sand; no odor				0.0		
6		ML	<i>Silt</i> Brown-gray; damp; mostly silt			HSA-1:4.5	- 0.0		
8- 			End of Boring			HSA-1:9	0.0		On Rock Refusal at 10' feet
12									
Di	rill Me	ethod	Cascade Drilling I: HSA 3402.0			1	<u> </u>	Hole Size: Datum: N/ Sheet: 1 o	AD83/98; NAVD88

Ø		VIR RTN	O N M E N T A L E R S I N C		E	Boring	j∕Well: M	<b>W-5</b>			
Clien	nt: Col	lony S	pecialty				Site Map			Ĩ	JEN
Loca	tion:	7833	SE 28th St Mercer Island, WA					H M	W-1 -	-	
Date	of Dr	illing:	9/10/12								
Logg	ged by	y: K. A	Addis						WW-5		
Tota	l dept	<b>h:</b> 20'	-	-				2	vivv-5		
			SUBSURFACE PROFILE	+			SAMPLE		_		
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Blow Counts	Sample	PID	Well Cor Deta	npletion ails	Comments
0_			Ground Surface	_					8	8	
		ML	Asphalt Silt	1						er -	
2		WILL .	Gray; moist; very stiff; mostly silt					0.2	Concrete	Traffic-rated monument	
6						9 13 18	MW-5:2.5	7.8	blank	Traffic-	
8									Sch. 40 PVC blank	Bentonite	
10			Becomes hard			18 24 29		0.2	5	teen T	
12									•	.010" PVC scre	
16		SP- SM	<b>Poorly-Graded Sand with Silt</b> Gray; saturated; very dense; mostly fine sand with few silt			21 50-6"	MW-5:15	0.3	10/20 Silca Sand	2" Sch 40 .0	17' ATD
18		SP- SM	<i>Poorly-Graded Sand with Silt</i> Gray; saturated; very dense; mostly fine sand			19			10		
20	a ta a fai ai ai		End of Boring			50-6"		0.0			
22											
24											
Dri	ill Meti	<b>y:</b> Cas hod: H t: 6340	ISA					D	lole Size: 8" Patum: NAD Theet: 1 of 1	83/98; N	AVD 88





Ø		VIR RTN	O N M E N T A L E R S I N C		E	Boring	/Well: N	IW-10			
Clier	nt: Co	lony S	pecialty				Site Map	1	MW	/-10	
Loca	tion:	7833	SE 28th St, Mercer Island WA					1	VAULT 1		
Date	of Dr	rilling	9/12/12						B-4		
Logg	ged by	<b>y:</b> K. A	Addis				E	3-3 ⊗ DI	<sup>2-8</sup> -0+	57	
Tota	l dept	t <b>h:</b> 25'	•				-				
			SUBSURFACE PROFILE				SAMPLE		-		
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Blow Counts	Sample	PID	Well Cor Det		Comments
0-			Ground Surface							<b></b> ×	
2		SW	Asphalt Well-Graded Sand with Gravel Brown; moist; mostly fine to coarse sand with some gravel and few silt					14	Concrete	I Casing	
4		ML	Silt					153	8	" Steel	
6		ML	Brown-gray; rust-stained; moist; mostly silt and clay with few gravel and sand	/]		27 50-6"	MW-10:6	1600	lite	1" 5	
8			Silt Gray; rust-stained; moist; hard; mostly silt and clay						Bentonite		
10		ML	<i>Silt</i> Gray; damp; hard; mostly silt	I		22 50-6"	MW-10:11	14.6	Ŧ	40 PVC blank	
14		ML	<b>Silt</b> Gray; damp; hard; mostly silt	Ī		50-6"		-	PVC screen	2" Sch. 40	
18-		ML	<i>Silt with Sand</i> Gray; damp; hard; mostly silt with few gravel and trace sand			27 50-6"	MW-10:21	18	- 2" Sch 40 .010"		
22		SP- SM	<b>Poorly-Graded Sand with Silt</b> gray; saturated; mostly fine to medium sand with silty sand seams 2"			29 50-6"		88			
26			End of Boring								
28-											
Dri	ill Met	<b>by:</b> Cas hod: H #: 6340						Da	ble Size: 8" atum: NAD heet: 1 of 1	83/98; NA	AVD 88

Ø	P A	VIR RTN	O N M E N T A L E R S I N C		E	Boring	j/Well: M	W-11				
Clien	t: Col	ony S	pecialty				Site Map			~		1
Loca	tion:	7833 :	SE 28th St Mercer Island, Wa								1	
Date	of Dr	illing:	9/11/12					MW-1	10		)	
Logg	ed by	/: K. A	ddis						•			V
Total	dept	<b>h:</b> 25'								1		
			SUBSURFACE PROFILE				SAMPLE		-			
Depth (ft)	Lithology	USCS Name	Description	Interval	Recovery	Blow Counts	Sample	PID		Comp Detail	oletion Is	Comments
0-			Ground Surface	_					8		8-	
			Asphalt								ent -	
2		SP- SM	<b>Poorly-Graded Sand with Silt</b> Rust-stained gray; moist; mostly fine to medium sand with few silt					12.6	Concrete		Traffic-rated monument	
4		ML	<i>Silt with Sand</i> Gray-blue; moist; hard; mostly silt				MW-11:3	12.0	ပိ		ed n	
			with some sand and few gravel	Л				2846			-rat	
6			(fill)			50-6"	MW-11:5.5	2010	lite		affic	
									Bentonite		Ē	
8		ML	<i>Silt with Sand</i> Gray; moist; hard; mostly silt with						Be			
10			little sand and trace gravel	Ш		50-6"		52.6			Ŧ	
12	1111111											
14											creen	
16		SM	<i>Silty Sand with Gravel</i> Gray; moist; very dense; mostly			50-6"	MW-11:15.5	14.0			õ	
18			fine sand with some silt and some gravel								0 .010" PVC	
20				I		50-4"		0.7			2" Sch 40	
22	UADANCHU	SP	<b>Poorly-Graded Sand with Gravel</b> Gray; saturated; very dense;								N 	
24		UI	mostly fine to medium sand and few gravel								<b>.</b>	
26			End of Boring	-11		50-6"		0.4				
28												
30-												
Dri	ll Meti	<b>y:</b> Cas h <b>od:</b> H <u>:</u> 6340	SA					Da	ole Size atum: N heet: 1	AD 8	3/98; N/	AVD88

eD	PAR	IRONMENTAL TNERSINC		BORING	ID: SVE-1		1 of 1
SITE AD	DDRESS			CLIENT:			CASING MATERIAL AND SIZE:
7833 \$	SE 28th	St, Mercer Island, WA		Colony Sp	ecialty		4" Sch 40 PVC Blank
				PROJECT #:			SCREEN SIZE:
Casca	cade Drilling, L.P.			63402.2		0.010"	
DRILLIN	NG EQUIP	MENT:		DATE:		SCREEN INTERVAL:	
CME-7	75			August 27	, 2013		3.5'-8.5'
DRILLIN	NG METHO	DD:		GROUND SU	RFACE ELEV. FT	AMSL:	FILTER PACK:
Air Kn	nife to 4	'; HSA (10") to 8.5'		92.14'			#2/12 Silica Sand
LOGGED BY: <b>K. Addis L.G.</b>			TOTAL DEPT	Ή:		FILTER PACK INTERVAL:	
	ais L.G.		>	8.5'			2.5'-8.5"
Depth (feet)	nscs	Description USCS name; Color; Moisture; Density; Plasticity; Dilatancy; EPI description; Other	Interval & % Recovery	Blows per 6"	Sample	PID (ppm)	Well Construction
	MH	GRAVEL BASE (6") SANDY ELASTIC SILT; reddish brown; damp; very stiff; non plastic; mostly silt with some sand, minor clay, and few gravel (Roots at 1' to 3') ELASTIC SILT WITH SAND; reddish gray; damp; very stiff; no plasticity; no dilatancy; mostly silt with minor clay, minor sand, and few gravel ELASTIC SILT; dark gray; damp; hard; medium plasticity; no dilatancy; mostly silt with minor clay, trace sand and trace gravel	80	9-14-18	SVE-1:5	1075 62 42	Traffic-rated monument with concrete surface seal Bentonite PVC blank Sand pack Well screen End Cap
10 - - 12 - - 14							

<b>edd</b>	E N V P A R	IRONMENTAL TNERS INC		BORING	ID: SVE-2		1 of 1
SITE ADI	DRESS			CLIENT:			CASING MATERIAL AND SIZE:
7833 S	E 28th	St, Mercer Island, WA		Colony Sp	ecialty		4" Sch 40 PVC Blank
DRILLING	G CONTE	RACTOR:		PROJECT #:			SCREEN SIZE:
Cascad	de Drill	ing, L.P.		63402.2		0.010"	
DRILLING	G EQUIP	MENT:		DATE:			SCREEN INTERVAL:
CME-7	5			August 27	, 2013		3'-8'
DRILLING	G METHO	DD:		GROUND SU	RFACE ELEV. FT	AMSL:	FILTER PACK:
		; HSA (10") to 8'		92.37'			#2/12 Silica Sand
LOGGED BY: <b>K. Addis L.G.</b>			TOTAL DEPT	Ή:		FILTER PACK INTERVAL: 2'-8'	
	IS L.G.		_ <u>&gt;</u>				2-0
Depth (feet)	NSCS	Description USCS name; Color; Moisture; Density; Plasticity; Dilatancy; EPI description; Other	Interval & % Recovery	Blows per 6"	Sample	PID (ppm)	Well Construction
0	MH	ASPHALT (3") GRAVEL OVER ASPHALT (3") (Mottled)	-				Traffic-rated monument with concrete surface seal
2 -		ELASTIC SILT WITH SAND; grayish brown; damp; hard; medium plasticity; slow dilatancy; mostly silt with minor clay and minor sand, trace gravel	-				Bentonite PVC blank
	MH						
			80	10-19-25	SVE-2:5	330	Sand pack
6		ELASTIC SILT; dark gray; damp; hard; medium plasticity; no dilatancy; mostly silt with minor clay and few sand	-				Well screen
8 -	MH		80	18-22-28	SVE-2:9	56	End Cap
10 -							
- 12 - -							
14 NOTES:	No grour	ndwater at time of drilling.					

	VIRONMENTAL RTNERS INC		BORING	ID: MW-128	5	1 of 1
SITE ADDRESS			CLIENT:			CASING MATERIAL AND SIZE:
7833 SE 28th	n St, Mercer Island, WA		Colony Sp	ecialty		2" Sch 40 PVC Blank
DRILLING CON			PROJECT #:			SCREEN SIZE:
Cascade Dri	lling, L.P.		63402.2			0.010"
DRILLING EQUI	PMENT:		DATE:			SCREEN INTERVAL:
CME-75			August 27	, 2013		5'-10'
DRILLING METH				RFACE ELEV. FT	AMSL:	FILTER PACK:
	5.4'; HSA (10") to 10'		92.02'			#2/12 Silica Sand
LOGGED BY: <b>K. Addis L.G</b>			TOTAL DEPT	H:		FILTER PACK INTERVAL: 3'-10'
		~ >			Ê	
Depth (feet) USCS	Description USCS name; Color; Moisture; Density; Plasticity; Dilatancy; EPI description; Other	Interval & % Recovery	Blows per 6"	Sample	PID (ppm)	Well Construction
0 2 - - - - - - - - - - - - -	ASPHALT (2") GRAVEL BASE (4") SILTY SAND WITH GRAVEL; dark greenish gray; moist; medium dense; mostly fine sand with some silt and minor gravel SANDY ELASTIC SILT; dark gray; moist; hard; medium plasticity; no dilantancy; mostly silt with some sand, minor clay, and trace gravel	100	10-11-10	MW-12S:6	1465	Traffic-rated monument with concrete surface seal Bentonite PVC blank Sand pack Well screen End Cap
- 14 NOTES: No grou	undwater at time of drilling.					

		IRONMENTAL TNERSINC		BORING	ID: MW-12	D	1 of 2
SITE ADD	DRESS			CLIENT:			CASING MATERIAL AND SIZE:
7833 SE	E 28th	St, Mercer Island, WA		Colony Sp	ecialty		2" Sch 40 PVC Blank
DRILLING	GCONTR	RACTOR:		PROJECT #:			SCREEN SIZE:
Cascad	le Drill	ing, L.P.		63402.2			0.010"
DRILLING	<b>GEQUIP</b>	MENT:		DATE:			SCREEN INTERVAL:
CME-75				August 28			20'-25'
DRILLING					RFACE ELEV. FT	AMSL:	FILTER PACK:
Air Knif		'; HSA (14") to 15'; HSA (8") to 25'		92.05' TOTAL DEPT	11.		#2/12 Silica Sand
K. Addi				25'	п.		18'-20'
			& v			Ê	
Depth (feet)	nscs	Description USCS name; Color; Moisture; Density; Plasticity; Dilatancy; EPI description; Other	Interval & % Recovery	Blows per 6"	Sample	PID (ppm)	Well Construction
0		ASPHALT (2") WITH GRAVEL BASE (4")					Traffic-rated
2	SM	SILTY SAND WITH GRAVEL; dark bluish gray; moist; medium dense; mostly fine sand with some silt and minor gravel	100	4-8-8		430	monument with concrete surface seal Bentonite
8 - - - - - - - - - - - - - - - - - - -	МН	ELASTIC SILT WITH GRAVEL; dark gray; dry; hard; medium plasticity; no dilatancy; mostly silt with minor clay, few gravel, and few sand; silty sand lens at 10.2'-10.5'	100	11-31-30		6.5	PVC blank

P A	VIRONMENTAL RTNERS INC		BORING	ID: MW-12I	C		2 of 2
TE ADDRESS	;		CLIENT:			CASING MATERIA	AL AND SIZE:
'833 SE 28t	n St, Mercer Island, WA		Colony Sp	ecialty	2" Sch 40 PVC Blank SCREEN SIZE:		
RILLING CON			PROJECT #:				
Cascade Dri	lling, L.P.		63402.2			0.010"	
RILLING EQU	PMENT:		DATE:			SCREEN INTERV	AL:
CME-75			August 28	, 2013		<b>20'-25'</b>	
RILLING MET				RFACE ELEV. FT	AMSL:	FILTER PACK:	
	5'; HSA (14") to 15'; HSA (8") to 2	5'	92.05'			#2/12 Silica Sa	
			TOTAL DEPT 25'	H:		FILTER PACK INT 18'-20'	ERVAL:
	Description	& /erv			Ê		
Depth (feet)	USCS name; Color; Moisture; Density; Plasticity; Dilatancy; EPI description; Othe	بت Interval & % Recoverv	Blows per 6"	Sample	PID (ppm)	WellCon	struction
	SANDY ELASTIC SILT WITH GRAVEL; gray; moist; hard; medium plasticity; no dilatency; mostly silt with some sand and gravel; silty sand lens at 16.0-16.3' satura lens	dark	20-22-24	MW-12D:16	0.2		Bentonite
- - 20 - - - -	As above; low plasticity; more silt than cla	ay 50	36-50/6"		0		Sand pack
22	POORLY-GRADED SAND; dark gray; we						Well scree
24 - - - SP	dense; mostly fine to medium sand with t gravel; organics at 26.0'-26.5'				0		
26 -	- - - - - -	100	16-17-20				End Cap

Date: 1/7/10	6		Soil Boring Log	Boring Name	e: MW-13		
Project Name:	Address:		t Name: Mercer Island Shell (Former BP)		I (Former BP)	Location:	
Address:			Northwest Corr of Intersection	ner			
Depth Blows	PID	USCS	Description		Well Construction		
- <b>5</b> - <b>1</b> - <b>10</b> - <b>1</b>	0.0	ML <sub>CL</sub>	Air knifed to 5 feet Moist to wet, medium to dark gray, Sample MW13-7	, silty clay to clayey silt			
-15 <sup>7</sup> 7777777777777777777777777777777	0.0	¥	Moist to wet, grayish-green and ta				
	0.0	SM	Saturated, medium gray, silty fine Dry to damp, greenish-gray, silty o	-	$\cdot \cdot \cdot \models \cdot \cdot$		
-20 -25 -30	MLCL		Total depth drilled = 16 feet		Well constructed of 2-inch-diameter PVC well casing with 0.010-inch screen 4 to 16 feet bgs 2/12 silica sand		
		Driller Nam	ne: Cascade Drilling/Curtis	Sampling Method: 3-inch x <sup>-</sup>	18-inch split spoon		
4616 25th Avenue NE #143		Drilling Me Diameter:	thod: Limited Access Hollow Stem Auger 8 inches	Weather Conditions: Cloudy, 40			

Date: 1/7	/16		Soil Boring Log	Boring Name	: MW-14		
Project Name	t Name: Mercer		ect Name: Mercer Island Shell (Former BP)		II (Former BP)	Location:	
Address:		E 28th Stree Island, Was	UT ITIETSECIUT		er		
Depth Blow	ws PID	USCS	Description		Well Construction		
- <b>5</b> - <b>1</b> 0 10 12 10 12 10 12 1 10 12 1 10 12 1 10 12 1 10 12 1 1 1 1 1 1 1 1 1 1 1 1 1	0.0	MĻ <sub>CL</sub>	Air knifed to 5 feet Damp to moist greenish-gray and dark Sample MW14-7.5 Wet, medium gray clay, medium plast As above, saturated Total depth drilled = 19 feet		Well constructed of 2-inch-diameter PVC well casing with 0.010-inch screen		
					4 to 19 feet bgs 2/12 silica sand		
PUGET		Driller Nar	ne: Cascade Drilling/Curtis S	ampling Method: 3-inch x 1	8-inch split spoon		
ENVIRONMENTAL P.L.L.C.     Drilling Method:     Weather Conditions:       4616 25th Avenue NE #143     Limited Access Hollow Stem Auger							

Date: 1/8/16	)		Soil Boring Log	Boring Name	: MW-15
Project Name:	Address: 7000 OF 00th Otreat		II (Former BP)	Location:	
			Southeast Corn of Intersection	er	
Depth Blows	PID	USCS	Description		Well Construction
<b>5</b>	0.0	MĻ <sub>CL</sub>	Air knifed to 5 feet Moist, blue-gray clay with silt, mediu Sample MW15-7.5 As above	m plasticity	
— <b>15</b> — <u>—</u> 27 27 50/6	0.0	<b>Y</b>	As above with interbedded coarse sa Saturated at 15 feet Total depth drilled = 15 feet	and and gravel	
-20					Well constructed of 2-inch-diameter PVC well casing with 0.010-inch screen 5 to 15 feet bgs
					2/12 silica sand
-35		Driller Nar	<sup>ne:</sup> Cascade Drilling/Curtis	Sampling Method: 3-inch x 1	8-inch split spoon
ENVIRONMENTAL P.L.L.C.		Weather Conditions: Cloudy, 40s			

Date:	8/31/16	3		Soil Boring Log	Boring Name	e: MW-16
Project Name: Mercer Island Shell (Forme		ell (Former BP)	Location:			
Address	:		E 28th Stre Island, Wa		North side of 2	8th Street
Depth Sample	Blows	PID	USCS	Description	•	Well Construction
	11 50/6 45 50/6 50/6	0.0 0.0 0.0		Air knifed to 5 feet Damp, medium grayish-brown, silty cla with trace gravel Damp, medium grayish-brown with ora clay to clayey silt with trace gravel Damp to wet, medium grayish-brown, s silt with trace gravel Saturated, medium gray, clayey silty fin	nge mottling, silty ilty clay to clayey	
⊥ 	50/6	0.0		Saturated, medium gray, clayey sity in Saturated, medium gray, clayey silty fin Total depth drilled = 19.5 feet		Well constructed of 2-inch-diameter PVC well casing with 0.010-inch screen
25	-					4.5 to 19.5 feet bgs 2/12 silica sand
_30 _35						
PUGE ENVIRO	ΝΜΕΝΤΑ		Driller Na Drilling N	Cascade Drining/Curus	Sampling Method: 3-inch x Weather Conditions:	18-inch split spoon
4616 25th Avenue NE #143 Seattle, Washington 98105 Project 15083-012916 JPM		Diameter	8 inches Cloudy, 50s		IS Page 1 of 1	

Date: 8/31/1	6		Soil Boring Log	Boring Name	e: MW-17
Project Name:	Mercer	Island She	ell (Former BP)	Location:	
Address:		E 28th Stre Island, Wa		North side of 2	8th Street
Depth Depth Blows	PID	USCS	Description		Well Construction
$ \begin{array}{c} -5 \\ -10 \\ -10 \\ -15 \\ -20 \\ -20 \\ -20 \\ -20 \\ -30 \\$	0.0 0.0 0.0	MLCL	Air knifed to 5 feet Damp to moist, grayish-tan, silty clay t Damp to moist, medium gray, silty clay Damp to moist, medium gray, silty clay Damp to moist, medium gray, silty clay Total depth drilled = 19.5 feet	y to clayey silt y to clayey silt	Well constructed of 2-inch-diameter PVC
—25—— —30——					well casing with 0.010-inch screen 4.5 to 19.5 feet bgs 2/12 silica sand
35	NE #143 1 98105	Driller N Drilling N Diameter	Method: Limited Access Hollow Stem Auger	Sampling Method: 3-inch x Weather Conditions: Cloudy, 50	

Date: 9/1/16			Soil Boring Log	Boring Name: M	W-18
Project Name:	Mercer I	sland She	ell (Former BP)	Location:	
Address:		28th Stre sland, Wa		East side of 80th Stree	et
Depth Blows	PID	USCS	Description	Well	Construction
$ \begin{array}{c} -5 \\ -10 \\ -10 \\ -15 \\ -15 \\ -20 \\ -20 \\ -20 \\ -25 \\ -30 \\ -35 \\$	3.0 0.5 0.0 0.0	ML <sub>CL</sub> ▼	Air knifed to 5 feet Damp to moist, medium grayish-brown clayey silt with trace gravel Moist to wet, bluish-gray, silty clay to c Saturated, bluish-gray, silty clay to clay Saturated, bluish-gray, silty clay to clay Saturated, bluish-gray, fine-grained sar Total depth drilled = 20 feet	layey silt ey silt rey silt ndy clayey silt Vell cor 2-inch-owell cas 0.010-ir 5 to 20 2/12 sili	nch screen feet bgs ca sand
PUGET ENVIRONMENTA	L P.L.L.C.	Driller Na	Cascade Drining/Curtis	Sampling Method: 3-inch x 18-inch	split spoon
4616 25th Avenue NE #143       Drilling Method:         Seattle, Washington 98105       Limited Access Hollow Stem Auger         Project 15083-012916 JPM       Diameter:		Weather Conditions: Cloudy, 50s	Page 1 of 1		

Date: 2/8/1	7		Soil Boring Log	Boring Name	: MW-20
Project Name:	Mercer	Island She	ell (Former BP)	Location:	
Address:		7833 SE 28th StreetWest Side of 80Mercer Island, WashingtonSouth of Site		West Side of 80 South of Site	th Avenue SE,
Depth <sup>ed</sup> Blows	PID	USCS	Description		Well Construction
$ \begin{array}{c}                                     $	0.0	ML <sub>CL</sub> ▼	Air knifed to 5 feet Damp, greenigh-gray and brownish-ora silty clay @ 8 feet, wet, grayish-green @ 16.5 feet, saturated As above, with fine-grained sand Saturated, dark gray, fine- to medium- Total depth drilled = 24 feet	grained sand, few fines	Well constructed of 2-inch-diameter PVC well casing with 0.010-inch screen 4 to 24 feet bgs 2/12 silica sand
35		Driller Na	ame: Cascade Drilling/Curtis	Sampling Method: 3-inch x 1	R_inch split spaan
ENVIRONMENT 4616 25th Avenue Seattle, Washingto	NE #143	Drilling N Diameter	Method: Limited Access Hollow Stem Auger	Weather Conditions: Rainy, 40s	o-mon spirt spoon
Project 15083-041417 JM			Page 1 of 1		

Date: 1/30/19			9	Soil Boring Log	Boring Nam	e: MW-21	
Proje	ct N	Name:	M	ercer Island Shell	Location:		
				3 SE 28th Street rcer Island, Washington	Northeas	t Corner	
Depth	Sample	Blows	PID	Description		Well Construction	
— 5 — —10—		35 50/6	0.0	Air-knifed to approximately 5 feet Moist, bluish gray, silty clay, trace fine-grained sand Sample B21-6 Moist to wet, bluish-gray silty clay with fine-grained sa	ınd.		
—15—				Total depth = 14 feet		Well constructed of 2-inch diameter PVC well casing with 0.010-inch screen	
-20-		-				2/12 silica sand	
—25—		-					
—30— —35—		-					
PUG				Driller Name: Cascade-Curtis	Sampling Method:		
E N V I I 4616 2	R O I 25th	N M E N T / Avenue N		Cascade-Curtis	3-inch Weather Conditions:	x 18-inch split spoon	
Seattle, Washington 98105 (206) 518-4887 PugetEnvironmental.com				Diameter: 8 inches	Cloudy Page <u>1</u> of <u>1</u>		

Date: 1/30/19			9	Soil Boring Log	Boring Nam	e: MW-22
Proje	ct N	Name:	M	ercer Island Shell	Location:	
Addre				33 SE 28th Street rcer Island, Washington	North Of Site In	SE 28th Street
Depth	Sample	Blows	PID	Description		Well Construction
— 5 — —10—		60/6	0.0	Air-knifed to approximately 5 feet Damp, light brown, fine-grained sand with cobbles and Sample B22-6	1 clay.	
-15		-		Total depth = 14 feet		Well constructed of 2-inch diameter PVC well casing with
-20-						0.010-inch screen 2/12 silica sand
-25-						
—30— —35—		· · ·				
PUG		T NMENT	AL P.L.L.C.	Driller Name: Cascade-Curtis	Sampling Method: 3-inch	x 18-inch split spoon
4616 2 Seattle	25th e, W	Avenue N /ashington	NE #143	Drilling Method: Hollow Stem Auger	Weather Conditions:	
(206) 518-4887 PugetEnvironmental.com			l.com	Diameter: 8 inches	Cloud	dy Page <u>1</u> of <u>1</u>

Date:		1/31/1	9	Soil Boring Log	Boring Nam	e: MW-23
Project Name: Me			Me	ercer Island Shell	Location:	
Addre				3 SE 28th Street cer Island, Washington	Southeast In 80	)th Avenue SE
Depth	Sample	Blows	PID	Description		Well Construction
— 5 — —10—		14 15 17	0.0	Air-knifed to approximately 5 feet Moist, bluish gray, silty clay, fine-grained sand. Sample B23-6		
—15—				Total depth = 14 feet		Well constructed of 2-inch diameter PVC well casing with 0.010-inch screen 2/12 silica sand
—20— —25—						
_30— _35—						
			AL P.L.L.C.	Driller Name: Cascade-Curtis	Sampling Method: 3-inch	x 18-inch split spoon
4616 2 Seattle	5th 9, W	Avenue N ashington	IE #143	Drilling Method: Hollow Stem Auger	Weather Conditions:	
(206) 518-4887 PugetEnvironmental.com			.com	Diameter: 8 inches	Cloud	dy Page <u>1</u> of <u>1</u>

Date: 1/31/19			9	Soil Boring Log	Boring Nam	e: MW-24	
Proje	ct N	lame:	Me	ercer Island Shell	Location:		
Addro				3 SE 28th Street cer Island, Washington	West Of Serv	vice Building	
Depth	Sample	Blows	PID	Description		Well Construction	
— 5 — —10—		35,50/ 5	0.0	Air-knifed to approximately 5 feet Wet, blueish-gray, silty clay, trace fine-grained sand. Sample B24-6, B24-7 Dry, light brown with orange mottling, silty clay, trace f sand.			
—15—				Moist to wet, bluish gray, silty clay with fine-grained sa Total depth = 14 feet	ind.	Well constructed of 2-inch diameter PVC well casing with 0.010-inch screen 2/12 silica sand	
—20— —25—							
—30— —35—							
			AL P.L.L.C.	Driller Name: Cascade-Curtis	Sampling Method: 3-inch	x 18-inch split spoon	
46162 Seattle	25th e, W	Avenue N ashingtor	NE #143	Drilling Method: Hollow Stem Auger	Weather Conditions:		
(206) 518-4887 PugetEnvironmental.com			.com	Diameter: 8 inches	Cloudy Page <u>1</u> of <u>1</u>		

# **APPENDIX B**

Allstructure Engineering Shoring Plan

# **GENERAL STRUCTURAL NOTES**

#### PROJECT SCOPE:

DESIGN IS FOR THE TEMPORARY SHORING FOR THE REMOVAL OF CONTAMINATED SOIL AT THE RPOJECT PROPERTY. THE TEMPORARY SHORING IS TO BE INSTALLED, INCLUDING THE TIEBACKS AND THE TESTING OF THE TIEBACKS, THEN THE CONTAMINATED MATERIAL IS TO BE EXCAVATED AND REPLACED WITH CLEAN STRUCTURAL FILL

**DESIGN CRITERIA:** DESIGN WAS BASED ON THE RECOMMENDATIONS OF THE CALIFORNIA TRENCHING AND SHORING MANUAL, SOI LOADING BASED ON GEOTECHNICAL REPORT DATED NOVEMBER 20,2020 BY SOUTH SOUND GEOTECHNICAL CONSULTING AND ADDITIONAL COMMUNICATIONS. THIS DESIGN IS NOT CONSIDERED COMPLETE UNTIL THE LOADING USED FOR THIS DESIGN IS REVIEWED AND APPROVED BY THE GEOTECHNICAL ENGINEER.

#### ACTIVE EARTH PRESSURE: 35 PCF PASSIVE EARTH PRESSURE: 300 PCF

SOIL ARCHING: 2X PILE DIAMETER SURCHARGE: 300 PSF TIE-BACK BOND STRENGTH: 1,000 PSF

#### EXISTING CONDITIONS:

THE CONTRACTOR SHALL FIELD VERIFY ALL EXISTING CONDITIONS, DIMENSIONS AND ELEVATIONS. THE CONTRACTOR SHALL NOTIFY THE ARCHITECT/ENGINEER OF ANY DISCREPANCIES FROM CONDITIONS SHOWN ON THE DRAWINGS PRIOR TO THE START OF THE WORK.

#### SUBMITTALS:

SHOP DRAWINGS SHALL BE SUBMITTED TO THE ARCHITECT/ENGINEER PRIOR TO FABRICATION AND CONSTRUCTION REGARDING ALL STRUCTURAL ITEMS, INCLUDING THE FOLLOWING:

STEEL FABRICATIONS AND TIEBACK ANCHORAGE INFORMATION

IF THE SHOP DRAWINGS DIFFER FROM, OR ADD TO THE DESIGN OF THE STRUCTURAL DRAWINGS, THEY SHALL BE CLEARLY IDENTIFIED. ANY CHANGES TO THE STRUCTURAL DRAWINGS SHALL BE SUBMITTED TO THE ARCHITECT/ENGINEER AND ARE SUBJECT TO REVIEW AND ACCEPTANCE OF THE ENGINEER.

#### <u>EARTHWORK</u>

PROTECT INCOMPLETE WORK FROM FLOODING DURING STORMS OR OTHER CAUSES, THOROUGHLY BRACE OR OTHERWISE PROTECT ALL STRUCTURES NOT STABLE AGAINST UPLIFT DURING CONSTRUCTION. TAKE ALL NECESSARY PRECAUTIONS TO PREVENT DISTURBANCE OF AND TO PROPERLY DRAIN THE AREAS UPON WHICH CONCRETE IS TO BE POURED. DO NOT ALLOW WATER TO ACCUMULATE IN EXCAVATIONS. REMOVE WATER TO PREVENT SOFTENING OF THE BASE FOUNDATIONS. CONVEY WATER REMOVED FROM THE EXCAVATIONS AND RAINWATER TO TEMPORARY DRAINAGE DITCHES OR OTHER STRUCTURES OUTSIDE THE EXCAVATION LIMITS FOR THIS STRUCTURE. ENSURE THAT THE WATERING OPERATIONS WILL NOT ADVERSELY EFFECT FOUNDATIONS. MAINTAIN THE EXCAVATION FREE FROM GROUND WATER FOR THE TIME REQUIRED TO COMPLETE THE WORK IN A PROPER WORKMANLIKE MANNER. REMOVE LOOSE OR DISTURBED SOIL FROM THE BOTTOMS OF EXCAVATION. FOOTINGS SHALL BEAR ON UNDISTURBED NATIVE SOIL OR COMPACTED STRUCTURAL FILL.

ALL STRUCTURAL AND MISCELLANEOUS STEEL: ASTM A36 (FY=36,000 PSI) UNLESS NOTED OTHERWISE

ALL WF STEEL: ASTM A992 (FY=50,000 PSI) T.S. COLUMN: ASTM A500, GRADE "B" (FY=46,000 PSI).

ALL BOLTS: ASTM A307 UNLESS NOTED OTHERWISE.

- WELDING: PER AWS STANDARDS. E70XX ELECTRODE AND BY AWS QUALIFIED WELDERS.
- ALL STEEL SHALL HAVE SHOP COAT IN ACCORDANCE WITH ARCHITECTURAL SPECIFICATIONS. ALL EXPOSED STEEL BELOW FINISH GRADE TO BE COATED WITH ASPHALTIC PAINT PRIOR TO BACKFILLING.

DESIGN, FABRICATION, AND ERECTION SHALL BE IN ACCORDANCE WITH THE "AISC SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS". WELDING SHALL CONFORM TO THE AWS CODES FOR ARC AND GAS WELDING IN BUILDING CONSTRUCTION AND SHALL BE 3/16" MINIMUM UNLESS OTHERWISE NOTED. WELDING SHALL BE BY AWS CERTIFIED WELDERS. PREQUALIFIED WELDING PROCEDURES ARE TO BE USED, UNLESS AWS QUALIFICATION IS SUBMITTED TO THE ARCHITECT/ENGINEER PRIOR TO FABRICATION.

#### PILE AND TIEBACK ANCHORS:

TIEBACK ANCHORS SHALL BE DRILLED IN "TITAN" INJECTION ANCHOR (30/16) OR ENGINEERED APPROVED ALTERNATIVE PLACED IN AN AUGERED HOLE HOLE USING CENTERING ELEMENTS EVERY 10 FEET. ANCHORS SHALL HAVE A PVC COVER TO FORM A NO-LOAD ZONE. FOR THE INJECTION ANCHOR THE RATE OF DRILLING SHALL BE SUCH THAT A 12" GROUT ANNULUS (GROUT BULB) IS FORMED AROUND THE TIE-BACK ANCHOR.

CEMENT SHALL BE ASTMC150, TYPE I OR II

CARE AND CONTROL OF SURFACE WATER RUN-OFF AND GROUND WATER SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.

THE CONTRACTOR SHALL IMMEDIATELY SUSPEND ACTIVITIES IF GROUND SUBSIDENCE IS OBSERVED IF THE WALL IS ADVERSELY AFFECTED.

**INSPECTION:** SPECIAL INSPECTIONS: IN ACCORDANCE WITH SECTION 1704 OF THE 2014 OSSC AND APPLICABLE SECTIONS OF THE PROJECT SPECIFICATIONS. SPECIAL INSPECTIONS ARE TO BE PERFORMED BY AN INDEPENDENT TESTING LABORATORY EMPLOYED BY THE OWNER FOR THE FOLLOWING AREAS OF WORK:

STEEL WELDING PILE INSTALLATION AND EXCAVATION PER GEOTECHNICAL ENGINEER

#### STRUCTURAL OBSERVATIONS:

STRUCTURAL OBSERVATIONS BY THE ENGINEER OF RECORD OR AN APPOINTED REPRESENTATIVE SHALL BE REQUIRED AT THE FOLLOWING TIMES DURING CONSTRUCTION:

NONE REQUIRED FIELD TESTING:

ANCHOR PROOF-LOAD TESTS AND VERIFICATION TEST SHALL BE PERFORMED IN GENERAL CONFORMANCE WITH THE LATEST EDITION OF THE RECOMMENDATIONS BY THE FEDERAL HIGHWAY ADMINISTRATION.

FOUR (4) GROUND ANCHOR SHALL BE PROOF-LOAD TESTED. TESTED ANCHORS SHALL HAVE A GROUTED LENGTH OF MORE THAN 10 FEET, BUT LESS THAN 15 FEET. PROOF TESTING LOAD (DTL) SHALL BE CALCULATED BASED ON THE ACTUAL GROUTED LENGTH: DTL - 2.97 KIPS/FOOT OF GROUTED LENGTH.

THE PROOF-LOAD TEST SHALL BE PERFORMED BY LOADING THE GROUND ANCHOR IN INCREMENTS OF 25% OF THE DESIGN LOAD TO A MAXIMUM LOAD (DTL). THE GROUND ANCHOR MOVEMENT WITH RESPECT TO AN INDEPENDENT FIXED REFERENCE (CREEP) SHALL BE MEASURED TO THE NEAREST 0.0001 INCH AT THE ALIGNMENT LOAD AND AT EACH INCREMENT OF LOAD. AT LOAD INCREMENT OTHER THAN THE MAXIMUM TEST LOAD, THE LOAD SHALL BE HELD JUST LONG ENOUGH TO OBTAIN THE READING.

THE MAXIMUM LOAD (DTL) SHALL BE HELD FOR TEN (10) MINUTES. THE JACK SHALL BE ADJUSTED AS NECESSARY IN ORDER TO MAINTAIN A CONSTANT LOAD. THE LOAD-HOLD PERIOD SHALL START AS SOON AS THE MAXIMUM TEST LOAD IS APPLIED TO THE GROUND ANCHOR MOVEMENT WITH RESPECT TO A FIXED REFERENCE (CREEP) SHALL BE MEASURED AND RECORDED AT 1 MINUTE, 2, 3, 4, 5, 6 AND 10 MINUTES. IF THE CREEP BETWEEN ONE (1) MINUTE AND TEN (10) MINUTES EXCEEDS 0.040 INCHES THE TEST LOAD SHALL BE HELD FOR AN ADDITIONAL 50 MINUTES. ANCHOR MOVEMENTS SHALL BE MEASURED AT 15, 20, 30, 40, 50 AND 60 MINUTES. THE CREEP VERSUS THE LOGARITHM OF TIME SHALL BE PLOTTED. IF THE CREEP RATE IS LESS THAN 0.080 INCHES BETWEEN 6 AND 60 MINUTES, THE TEST SHALL BE CONSIDERED SUCCESSFUL.

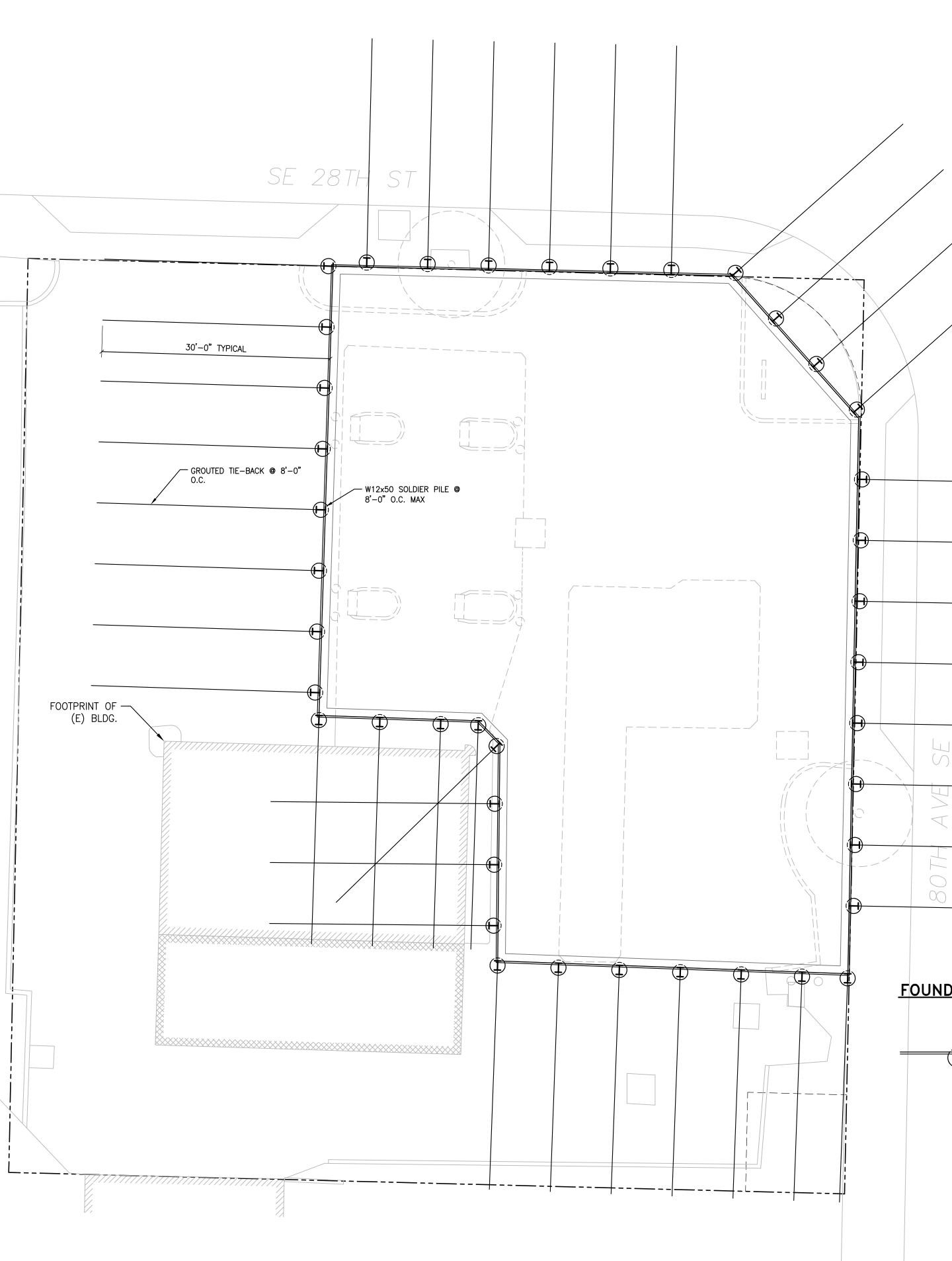
ANCHORS THAT DO NOT SATISFY THE ACCEPTANCE CRITERIA SHALL BE REPLACED OR REDESIGNED OR RETESTED.

ONE (1) GROUND ANCHOR SHALL BE VERIFICATION TESTED. TESTED ANCHORS SHALL HAVE A GROUTED LENGTH OF MORE THAN 10 FEET, BUT LESS THAN 14.5 FEET. VERIFICATION TESTING LOAD (VTL) SHALL BE CALCULATED BASED ON THE ACTUAL GROUTED LENGTH: DTL = 3.996 KIPS/FOOT OF GROUTED LENGTH. LOADS SHALL BE APPLIED IN ACCORDANCE WITH THE ATTACHED SCHEDULE.

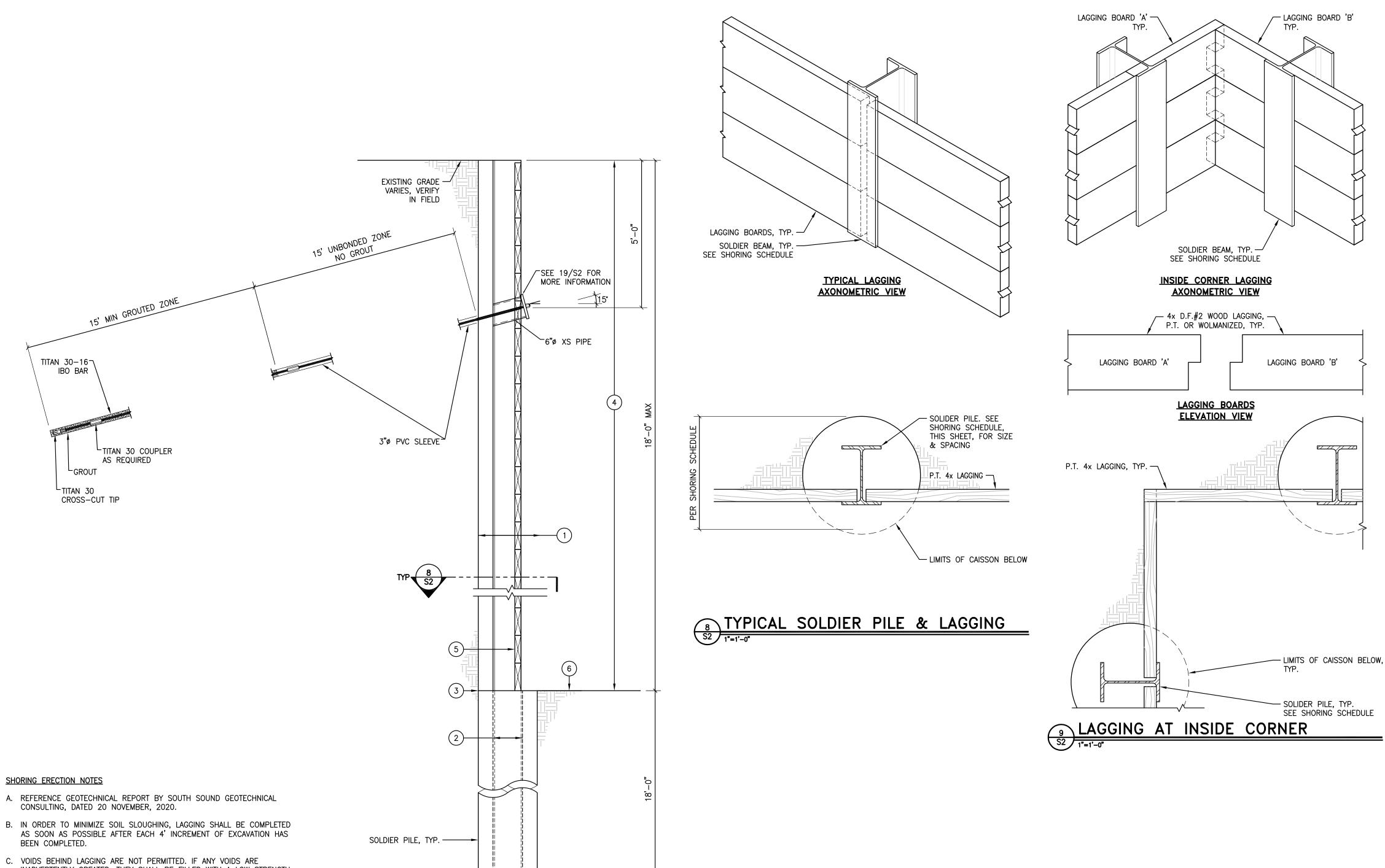
HOLD EACH LOAD INCREMENT FOR AT LEAST 10 MINUTES. MONITOR THE VERIFICATION TEST NAIL FOR CREEP AT THE VTL LOAD INCREMENT. MEASURE AND RECORD NAIL MOVEMENTS DURING THE CREEP PORTION OF THE TEST IN INCREMENTS OF 1 MINUTE, 2, 3, 5, 6, 10, 20, 30, 50 AND 60 MINUTES. MAINTAIN THE LOAD DURING THE CREEP TEST WITHIN 2 PERCENT OF THE INTENDED LOAD BY USE OF THE LOAD CELL. IF THE MOVEMENT IS LESS THAN 0.08 INCHES BETWEEN THE 6 AND 60 MINUTE READINGS AND THE CREEP RATE IS LINEAR OR DECREASING THROUGHOUT THE CREEP TEST LOAD HOLD PERIOD THE TEST IS CONSIDERED SUCCESSFUL. IF PULL OUT FAILURE DOES NOT OCCUR AT THE END OF THE VERIFICATION TEST THEN THE TEST IS CONSIDERED SUCCESSFUL. PULLOUT IS DEFINED AS THE CONTINUED MOVEMENT OF THE TEST LOAD WITH THE INABILITY TO FURTHER INCREASE THE TEST LOAD. RECORD THE PULLOUT FAILURE LOAD AS PART OF THE TEST DATA.

FOOTPRINT OF . (E) BLDG.

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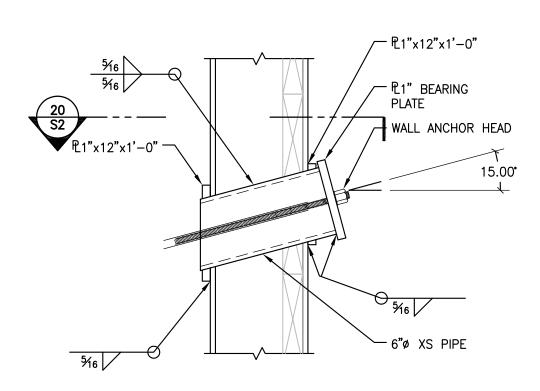
	ALLSTRUCTURE         Bingineering       LLC         16154 SW Upper Boones Ferry Rd • Portland, Oregon 97224         v: 503.620.4314 • f: 503.620.4304 • www.allstructure.com
	EXPIRES 11/7/ 2021
	MERCER ISLAND SHELL ALTERATION/REHABILITATION MERCER ISLAND, WA
DATION PLAN LEGEND Soldier Pile, spacing per plan. see sheet s2 For typical shoring details	GENERAL NOTES SHORING PLAN
TIE-BACK ANCHOR	HESE DRAWINGS ARE THE PROPERTY OF ALLSTRUCTURE ENGINEERING LLC AND ARE NOT TO BE USED OR REPRODUCED IN ANY MANNER EXCEPT WITH THE PROPER WRITTEN PERMISSION OF ALLSTRUCTURE ENGINEER ING LLC. DATE: 01.20.2021 SHEET SIZE: 24x36 DRAWN BY: RH CHK'D BY: RH SHEET SHEET SHEET SHEET DRAWN BY: RH CHK'D BY: RH

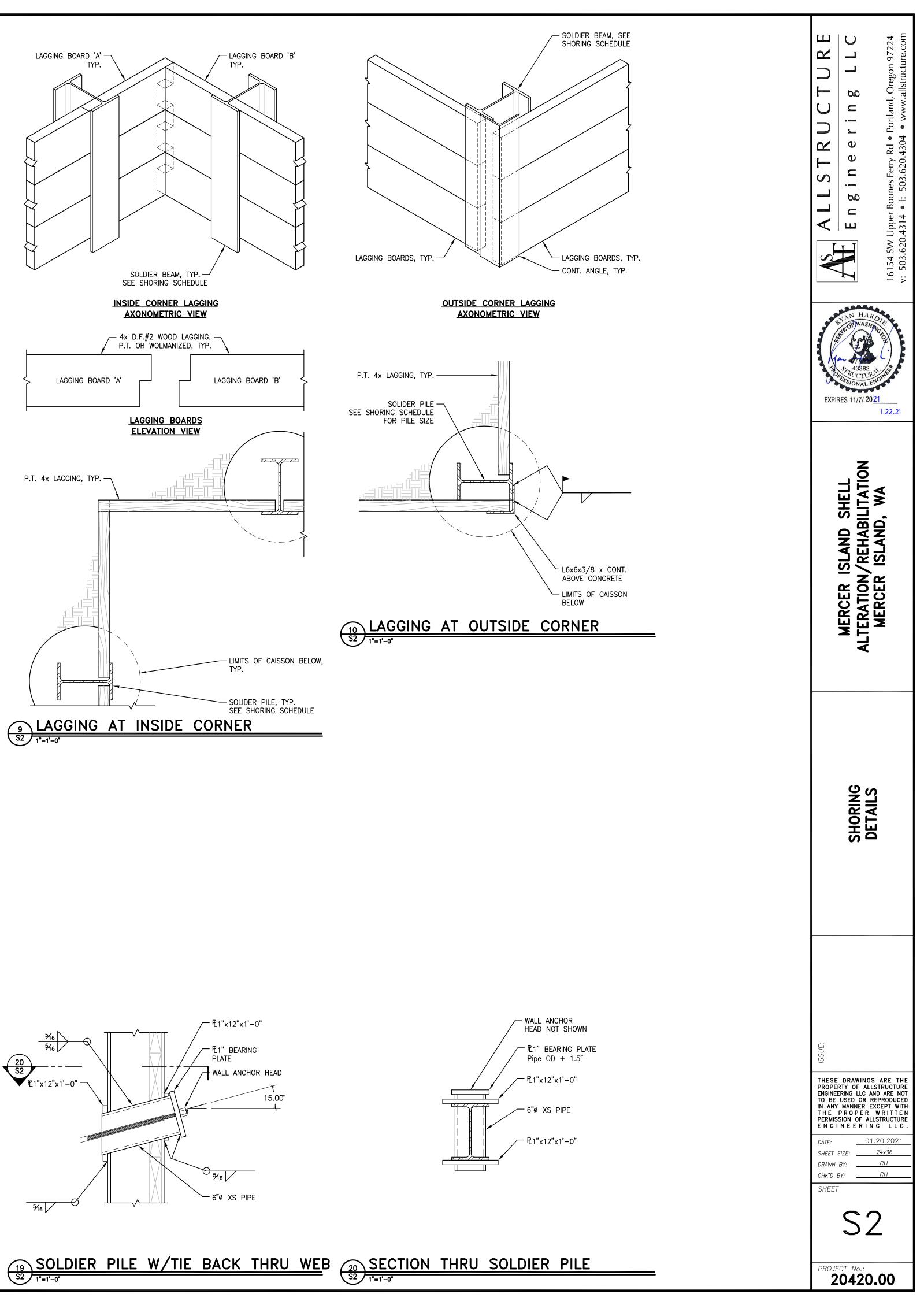


- INADVERTENTLY CREATED, THEY SHALL BE FILLED WITH A LOW STRENGTH SAND/CEMENT SLURRY.
- D. ANY LAGGING LEFT IN PLACE SHALL BE PRESSURE-TREATED WITH CREOSOTE OR SIMILAR SUBSTANCE TO IMPEDE WOOD DETERIORATION.
- SHORING ERECTION PROCEDURE
- 1. DRILL CAISSONS TO DEPTHS INDICATED IN SHORING SCHEDULE.
- 2. PLACE SOLDIER PILES. W12X50, TYPICAL UNO.
- 3. FILL CAISSON TO BOTTOM OF FOOTING ELEVATION WITH 2000 PSI CONCRETE AND THE REMAINDER OF THE HOLE WITH LEAN CONCRETE OR SOIL CEMENT AND ALLOW TO SET FOR 48 HOURS.
- 4. EXCAVATE EXISTING SOIL TO LIMITS INDICATED AT 4'-0" MAX. OR AS DIRECTED BY GEOTECHNICAL ENGINEER.
- 5. PLACE 6x LAGGING. REPEAT STEPS 4 THRU 5 UNTIL EXCAVATION IS COMPLETED TO BOTTOM OF FOOTING ELEVATION.
- 6. LIMITS OF EXCAVATION PROVIDED FOR REFERENCE ONLY. SEE PLANS. ACTUAL LIMITS OF EXCAVATION TO BE DETERMINED IN FIELD. CONTACT EOR IF LIMITS DEVIATE SIGNIFICANTLY FROM THE PLANS.

# 6 SOLDIER PILE NOTES







# **APPENDIX C**

Report Limitations and Guidelines for Use

# **REPORT LIMITATIONS AND USE GUIDELINES**

#### **Reliance Conditions for Third Parties**

This report was prepared for the exclusive use of the Client. No other party may rely on this report or the product of our services without the express written consent of Aspect Consulting, LLC (Aspect). This limitation is to provide our firm with reasonable protection against liability claims by third parties with whom there would otherwise be no contractual conditions or limitations and guidelines governing their use of the report. Within the limitations of scope, schedule and budget, our services have been executed in accordance with our Agreement with the Client and recognized standards of professionals in the same locality and involving similar conditions.

#### Services for Specific Purposes, Persons and Projects

Aspect has performed the services in general accordance with the scope and limitations of our Agreement. This report has been prepared for the exclusive use of the Client and their authorized third parties, approved in writing by Aspect. This report is not intended for use by others, and the information contained herein is not applicable to other properties.

This report is not, and should not, be construed as a warranty or guarantee regarding the presence or absence of hazardous substances or petroleum products that may affect the subject property. The report is not intended to make any representation concerning title or ownership to the subject property. If real property records were reviewed, they were reviewed for the sole purpose of determining the subject property's historical uses. All findings, conclusions, and recommendations stated in this report are based on the data and information provided to Aspect, current use of the subject property, and observations and conditions that existed on the date and time of the report.

Aspect structures its services to meet the specific needs of our clients. Because each environmental study is unique, each environmental report is unique, prepared solely for the specific client and subject property. This report should not be applied for any purpose or project except the purpose described in the Agreement.

### **This Report Is Project-Specific**

Aspect considered a number of unique, project-specific factors when establishing the Scope of Work for this project and report. You should not rely on this report if it was:

- Not prepared for you
- Not prepared for the specific purpose identified in the Agreement
- Not prepared for the specific real property assessed
- Completed before important changes occurred concerning the subject property, project or governmental regulatory actions

If changes are made to the project or subject property after the date of this report, Aspect should be retained to assess the impact of the changes with respect to the conclusions contained in the report.

#### **Geoscience Interpretations**

The geoscience practices (geotechnical engineering, geology, and environmental science) require interpretation of spatial information that can make them less exact than other engineering and natural science disciplines. It is important to recognize this limitation in evaluating the content of the report. If you are unclear how these "Report Limitations and Use Guidelines" apply to your project or site, you should contact Aspect.

#### **Discipline-Specific Reports Are Not Interchangeable**

The equipment, techniques and personnel used to perform an environmental study differ significantly from those used to perform a geotechnical or geologic study and vice versa. For that reason, a geotechnical engineering or geologic report does not usually address any environmental findings, conclusions or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. Similarly, environmental reports are not used to address geotechnical or geologic concerns regarding the subject property.

## **Environmental Regulations Are Not Static**

Some hazardous substances or petroleum products may be present near the subject property in quantities or under conditions that may have led, or may lead, to contamination of the subject property, but are not included in current local, state or federal regulatory definitions of hazardous substances or petroleum products or do not otherwise present potential liability. Changes may occur in the standards for appropriate inquiry or regulatory definitions of hazardous substance and petroleum products; therefore, this report has a limited useful life.

# **Property Conditions Change Over Time**

This report is based on conditions that existed at the time the study was performed. The findings and conclusions of this report may be affected by the passage of time (for example, Phase I ESA reports are applicable for 180 days), by events such as a change in property use or occupancy, or by natural events, such as floods, earthquakes, slope failure or groundwater fluctuations. If more than six months have passed since issuance of our report, or if any of the described events may have occurred following the issuance of the report, you should contact Aspect so that we may evaluate whether changed conditions affect the continued reliability or applicability of our conclusions and recommendations.

#### Phase I ESAs – Uncertainty Remains After Completion

Aspect has performed the services in general accordance with the scope and limitations of our Agreement and the current version of the "Standard Practice for Environmental Site Assessments: Phase I Environmental Site Assessment Process", ASTM E1527, and U.S. Environmental Protection Agency (EPA)'s Federal Standard 40 CFR Part 312 "Innocent Landowners, Standards for Conducting All Appropriate Inquiries".

No ESA can wholly eliminate uncertainty regarding the potential for recognized environmental conditions in connection with subject property. Performance of an ESA study is intended to reduce, but not eliminate, uncertainty regarding the potential for environmental conditions affecting the subject property. There is always a potential that areas with contamination that were not identified during this ESA exist at the subject property or in the study area. Further evaluation of such potential would require additional research, subsurface exploration, sampling and/or testing.

#### **Historical Information Provided by Others**

Aspect has relied upon information provided by others in our description of historical conditions and in our review of regulatory databases and files. The available data does not provide definitive information with regard to all past uses, operations or incidents affecting the subject property or adjacent properties. Aspect makes no warranties or guarantees regarding the accuracy or completeness of information provided or compiled by others.

#### Exclusion of Mold, Fungus, Radon, Lead, and HBM

Aspect's services do not include the investigation, detection, prevention or assessment of the presence of molds, fungi, spores, bacteria, and viruses, and/or any of their byproducts. Accordingly, this report does not include any interpretations, recommendations, findings, or conclusions regarding the detection, assessment, prevention or abatement of molds, fungi, spores, bacteria, and viruses, and/or any of their byproducts. Aspect's services also do not include the investigation or assessment of hazardous building materials (HBM) such as asbestos, polychlorinated biphenyls (PCBs) in light ballasts, lead based paint, asbestos-containing building materials, urea-formaldehyde insulation in on-site structures or debris or any other HBMs. Aspect's services do not include an evaluation of radon or lead in drinking water, unless specifically requested.